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DETAILED ENGINEERING EVALUATION

123 BLENHEIM ROAD

CHRISTCHURCH

ISSUE 2

14th Oct 2014

JOB NO: 140073



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INTRODUCTION

This report has been prepared for Paul Brown for the property at 123 Blenheim Rd. The report details the results found from an engineering investigation into the performance of the building in the recent earthquakes, and its likely structural capacity for future events.

The format of the investigation and the reporting is in accordance with the “Guidance on Detailed Engineering Evaluation of Earthquake Affected Non-residential Buildings in Canterbury”, Part 2. (Labelled as DEE in future references in this report)

WORK COMPLETED

The work completed consists of:

- The gathering of existing building information. This involved searching for existing plans and checking the structure on site against these plans.
- A detailed damage inspection has been carried out checking damage sustained from the recent earthquakes.
- Floor levels were checked on site to determine any areas of excessive settlement.
- A qualitative assessment has been carried out to determine a structural earthquake strength of the building comparative to the new building standard(%NBS)
- No invasive investigation was required as the structure was identifiable from the existing plans and visible on site.

BUILDING INFORMATION

Address 123 Blenheim Rd
Riccarton, Christchurch, 8041

Usage Ground floor – Commerical Use
First floor – Commercial Use

No. of Storeys 2

Building Dimensions Total dimensions 37m x 30m (Area approx. 790m²)

Year of construction 1993

Foundations Various size concrete post hole foundations situated under portal frame legs and tied to adjacent post hole over the full width of the slab with 2-H16 bar ties.
Strip footings run underneath the concrete panels typically 200mm wide.
Gravity load pad foundation under the first floor support column in the southern unit.

Floor The first floor structure consists of 75mm Unispan units with 75mm topping containing 665 reinforcing mesh. The unispan units have a minimum seating of 15mm. The 75mm topping slab is tied into the ground floor wall panels with D10 starters at 275mm centres.

The ground floor consists of a 125mm unreinforced poured concrete slab.

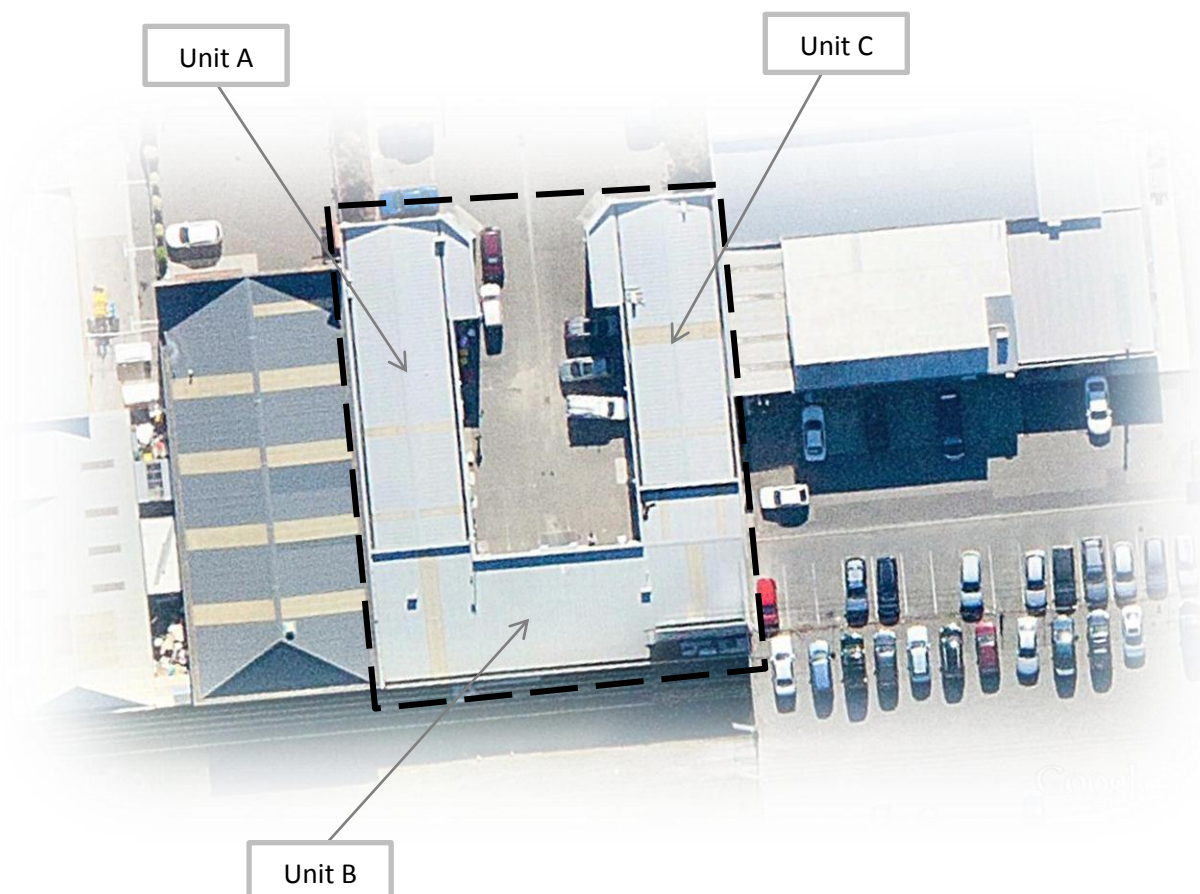
Walls 120mm precast concrete wall panels reinforced with 663 mesh.
Wall panels contain 2 layers of 663 mesh at pier locations and typically additional D12 reinforcing bars.
250UB portals span the 8.1m width in the single storey units.

Roof The roof structure comprises of lightweight iron cladding on BP150/19 purlins spanning between the UB portal rafters and precast concrete wall panels.

Structural System The gravity load system comprises of the portal frames and concrete precast panels. The unispan first floor slab distributes the first floor load to the ground floor panels and into the foundations.

The main lateral load resisting system in both directions consists of the precast concrete panels in plane. First floor loads are picked up through starter bars connected into the concrete panels.

The steel portal frames are also a main part of the lateral load resisting system in the east/west direction.



SITE PLAN- 123 BLENHEIM ROAD

BUILDING HOT SPOTS

The evaluation has been completed using Appendix A of the DEE guidelines.

The building has been reviewed to determine potential “hot spots” in the structural system. As the building consists of predominantly concrete precast wall panels and steel portal frames, the following areas are of concern:

<u>Potential Issue</u>	<u>Observation of the performance</u>
Inadequate foundations	The foundations have performed well. The site has not sustained large amounts of settlement or liquefaction. Only minor gradients were noted <1:350 and each unit was found to be within 10-20mm.
Inadequate face load capacity of precast wall panels	The precast panels were found to contain non ductile reinforcing mesh. As a result, the panels have been assessed at a ductility level of 1.25. The calculated strength of the concrete panels in face loading is 73%NBS. Widespread cracking up to 0.5mm is visible in all units. These are typically vertical cracks at the mid-span location of each panel. Panel 5 in Unit B has displaced by up to 18mm at the mid-span. This can be observed at ground level where the panel has separated from the ground floor slab. It is recommended that the concrete panels are repaired back to pre-earthquake condition using epoxy injection techniques.
Excessive deflection of portal frame during in plane loading	No excessive deflections were witnessed to the portal frames. No pounding damage was observed to the neighbouring buildings as a result of excessive deflections.
Inadequate panel connections	Panel connections appear in sound structural condition where inspected. No structural damage was witnessed to bolted connections.
Inadequate in plane capacity of concrete precast panels	Diagonal cracking was noted to several concrete panels around openings. This type of damage is typical for concrete panels having experienced large shear forces. The panels can be repaired back to pre-earthquake strength using epoxy injection.

BUILDING STRUCTURAL STRENGTH COMPLIANCE

Detailed structural calculations have been carried out to determine the seismic capacity of the building relative to the new building standard (%NBS).

The capacity of the critical structural elements in the lateral load resisting systems has been checked.

The building has a structural seismic capacity of approximately 73%NBS.

SUMMARY

The building has sustained a reasonable amount of structural damage to the concrete wall panels during the recent earthquake events. The cracking in the wall panels is due to face load deflection during seismic loading.

It has been concluded that the building has a strength of approximately 73%NBS.

The floor slab settlement throughout the building is minor.

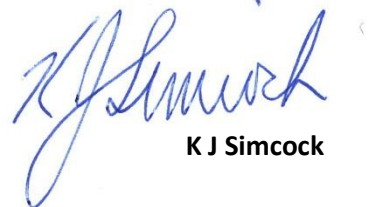
Structural repair is to be carried out as stated in appendix 2.



Michael Hughes

TM CONSULTANTS LTD

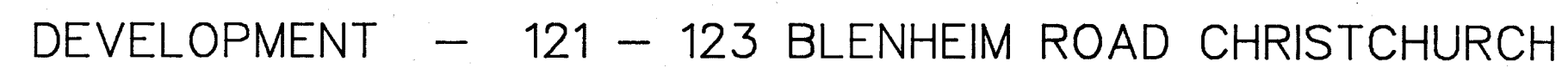
Checked and approved by



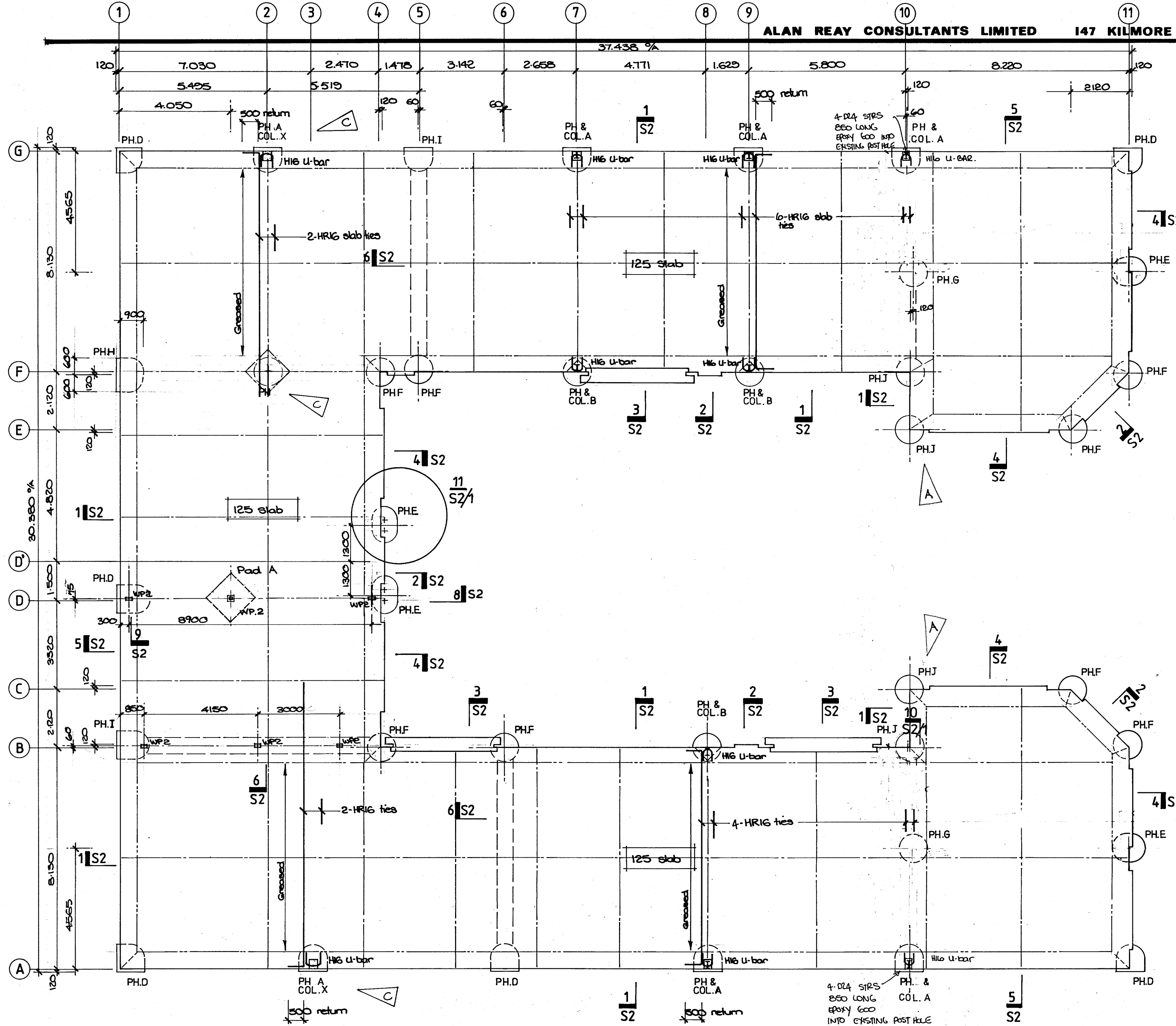
K J Simcock

Appendix 1

Building Plans



DRN	W.L.S.	APPROVED	DATE	SCALES	FLOOR PLAN	SHEET	FILE
DES			JUNE 1993	1:100		S01	4860
CKD							



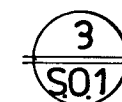
NOTES

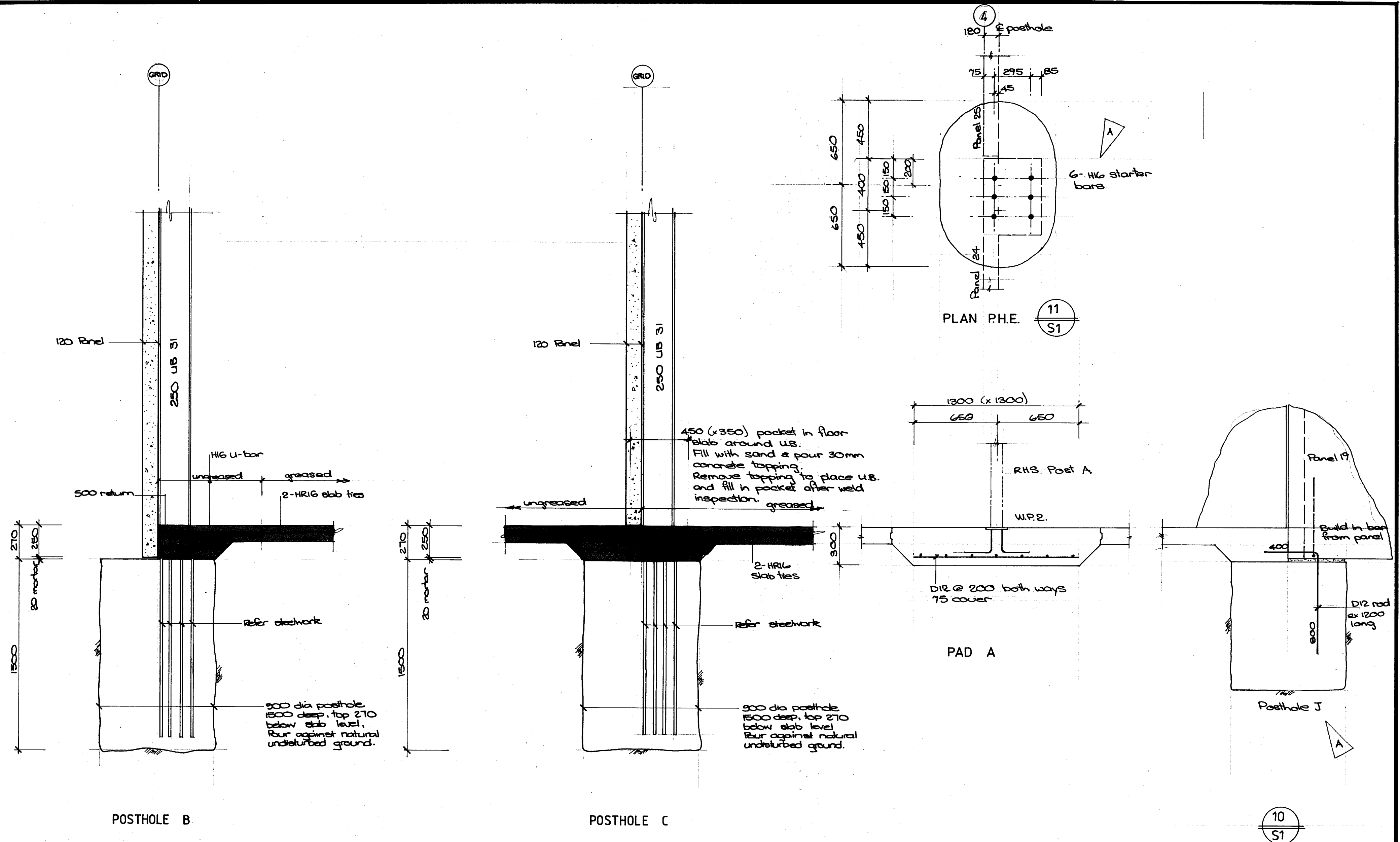
- Contractor to verify all dimensions on site BEFORE commencing works.
- Refer to the Architectural drawings for all nibs, rebates, fixings, holes etc.
- Pour all foundations against natural undisturbed ground. Carry all foundations to solid bearing.
- Contractor to determine positions of all building services ie., sewer, stormwater, power, telephone cables etc., before pouring foundations.
- Slab Joints
Denotes saw-cut or formed joint. Joint sealant is to be installed after slab shrinkage has taken place, and no sooner than 6 months after pouring slabs. For saw-cut joints install a temporary filler, to be removed when sealants shown are installed.
- POSTHOLES:
- Posthole D
- 900 dia posthole, 1500 deep, top 270 below slab level. Square off to boundary, pour against natural undisturbed ground.
- Posthole E
- 2 - 900 dia postholes, 400 apart, 1500 deep, top 270 below slab level. Pour against natural undisturbed ground.
- Posthole F
- 900 dia posthole, 1000 deep, top 270 below slab level. Pour against natural undisturbed ground.
- Posthole G
- 900 dia posthole, 1500 deep, top 125 below slab level. Pour against natural undisturbed ground.
- Posthole H
- 2 - 900 dia postholes, 300 apart, 1500 deep, top 270 below slab level. Square off to boundary, pour against natural undisturbed ground.
- Posthole I
- 900 dia posthole, 1000 deep, top 270 below slab level. Square off to boundary. Pour against natural undisturbed ground.
- Posthole J
- 900 dia posthole, 1000 deep, top 270 below slab level. Pour against natural undisturbed ground. These postholes to have D12 starter rod. Refer Section 10 on sheet S2/1

DEVELOPMENT - 121 - 123 BLENHEIM ROAD CHRISTCHURCH

DRN	CPL	APPROVED	DATE	SCALES	SHEET	FILE
DES			JUNE 1993	1:100	FOUNDATION PLAN	S1 4860
CKD						

A 20/1/93 Added Posthole J's.
B 11-8-93 COL A'S ADDED AT 10-A & 10-G, WP'S & THICKENING DELETED.
C 30-8-93 2-COL A'S, 1 COL C DELETED, 2-COL Y ADDED



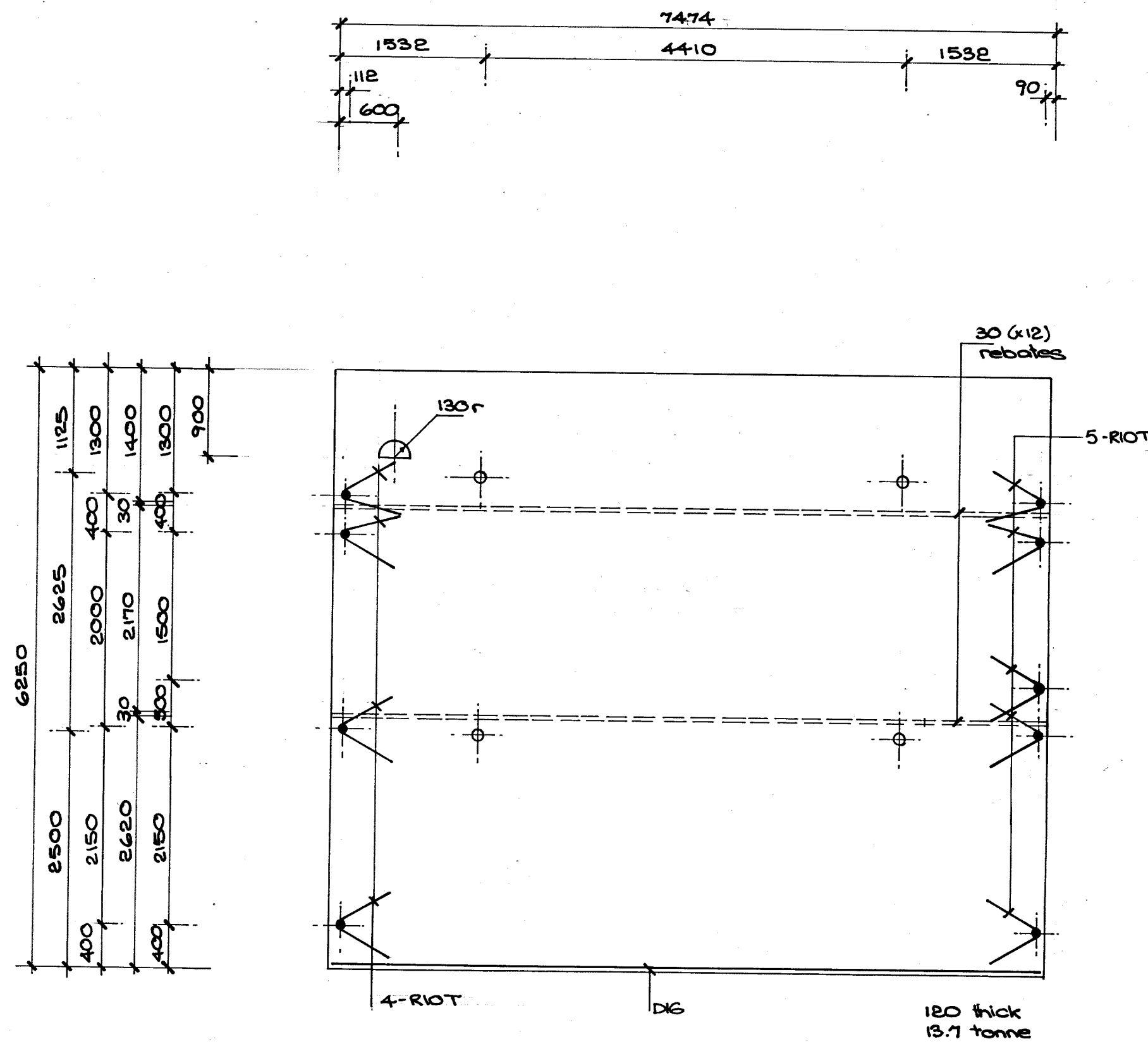


Refer to sheet S1 for notes

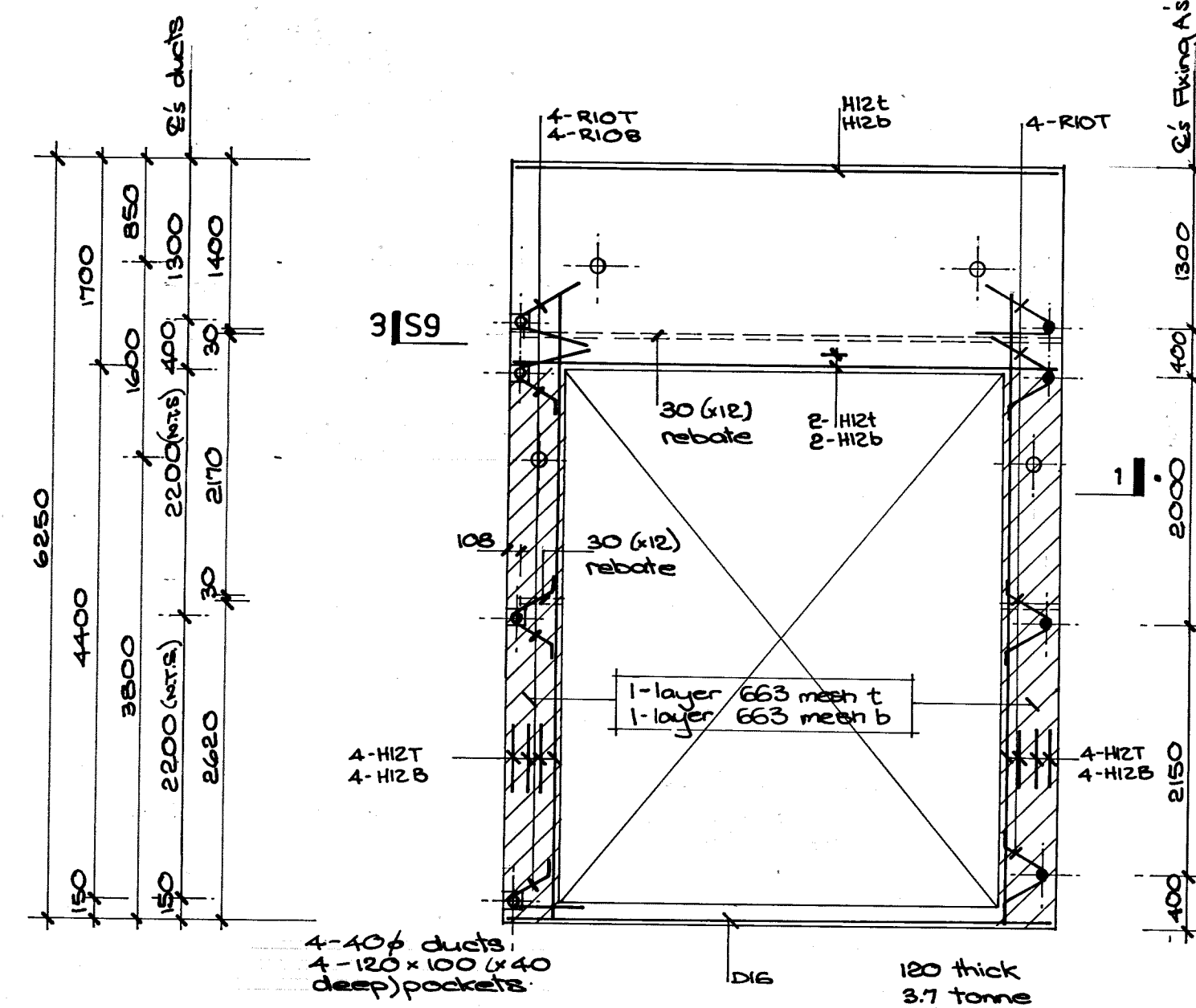
DEVELOPMENT — 121 — 123 BLENHEIM ROAD CHRISTCHURCH

DRN	DES	CKD	APPROVED	DATE	SCALES	SHEET	FILE
				JUNE 1993	1:20	FOUNDATION DETAILS	
						S2/1	4860

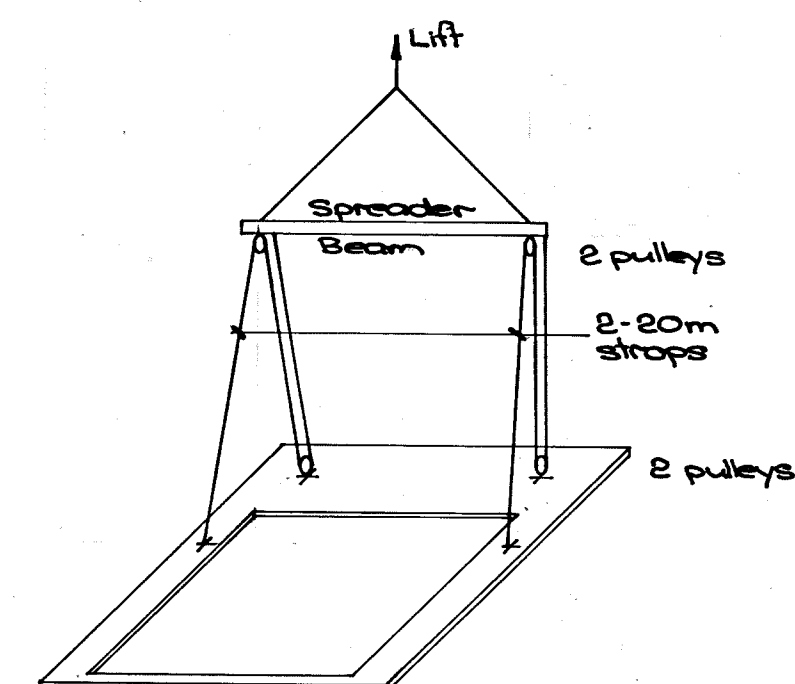
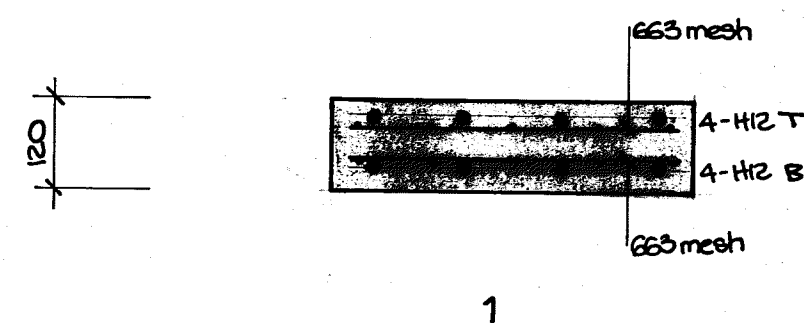
A 20/1/93 Changed D12 starters to H16, Section 11
 Changed Posthole F to J, Section 10



PANEL 21



PANEL 22



LIFTING DIAGRAM PANEL 22

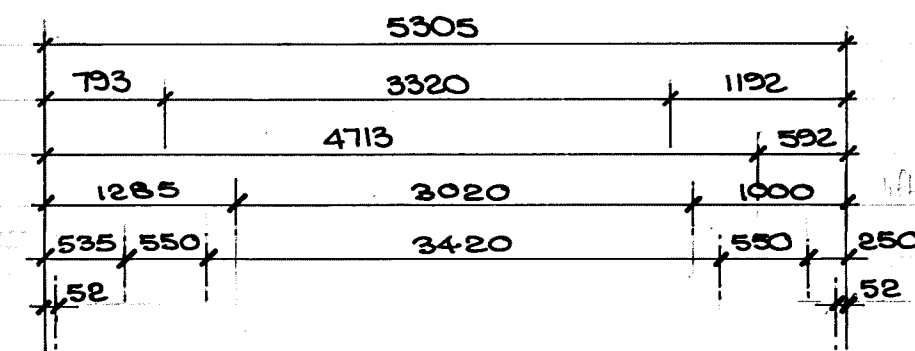
Refe: to sheet S3 for notes

DEVELOPMENT — 121 — 123 BLENHEIM ROAD CHRISTCHURCH

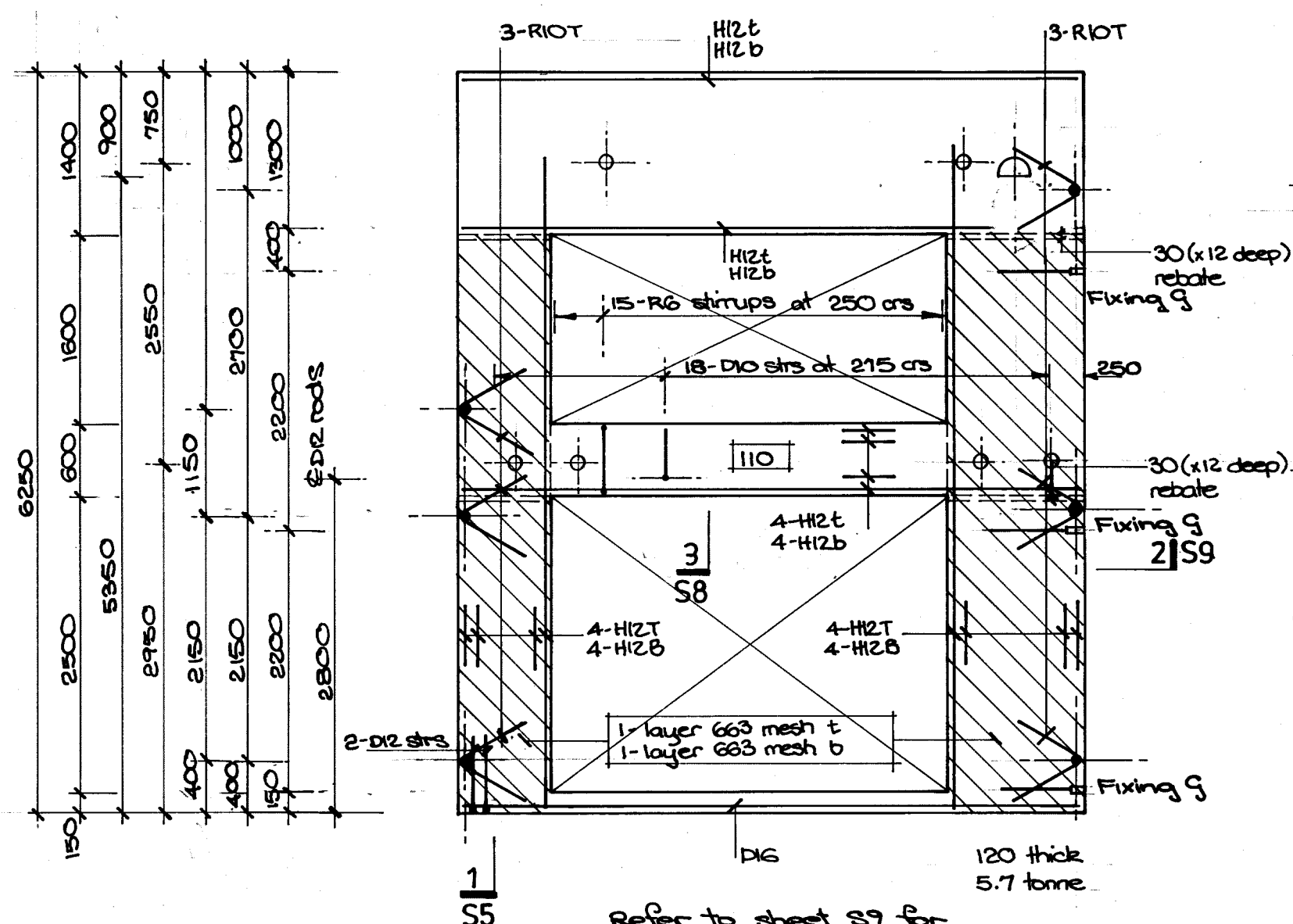
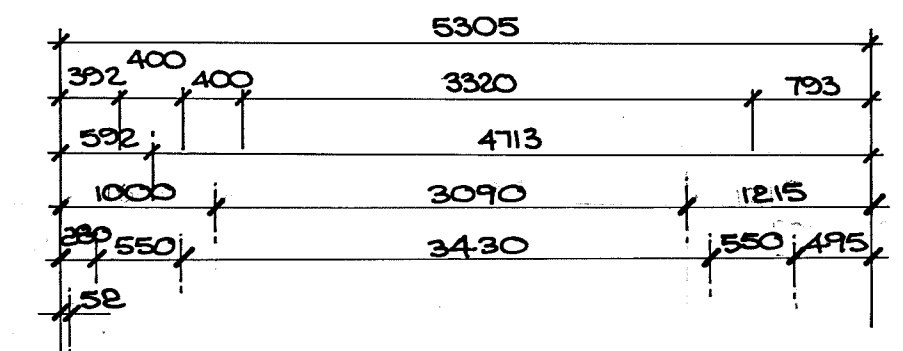
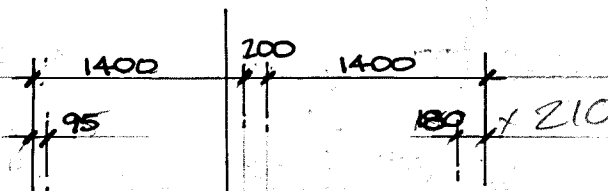
DRN	W.L.S.	APPROVED	DATE	SCALES
DES			JUNE 1993	1:50
CKD				

PRECAST CONCRETE
PANELS 21 & 22

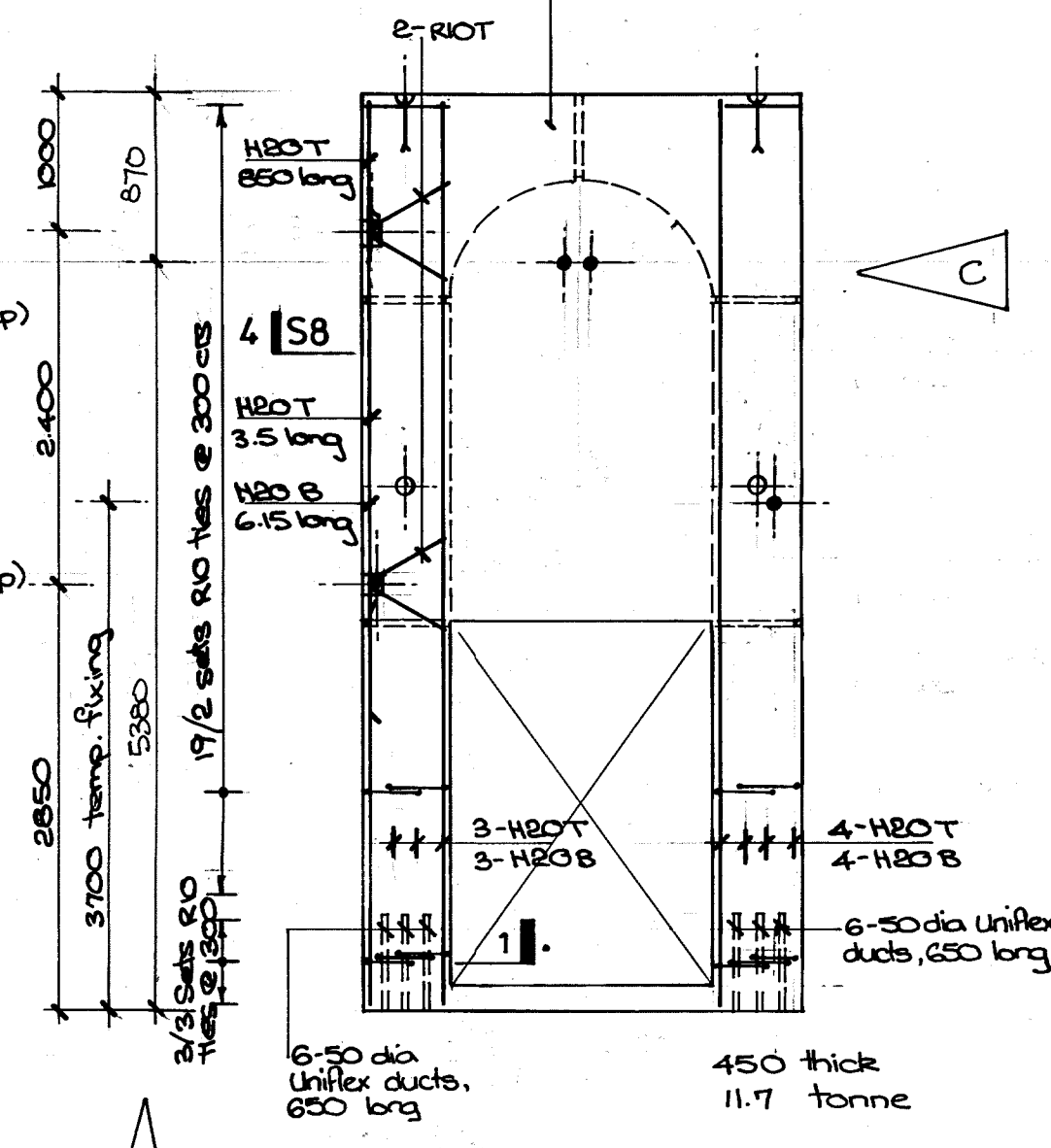
SHEET	FILE
S10	4860



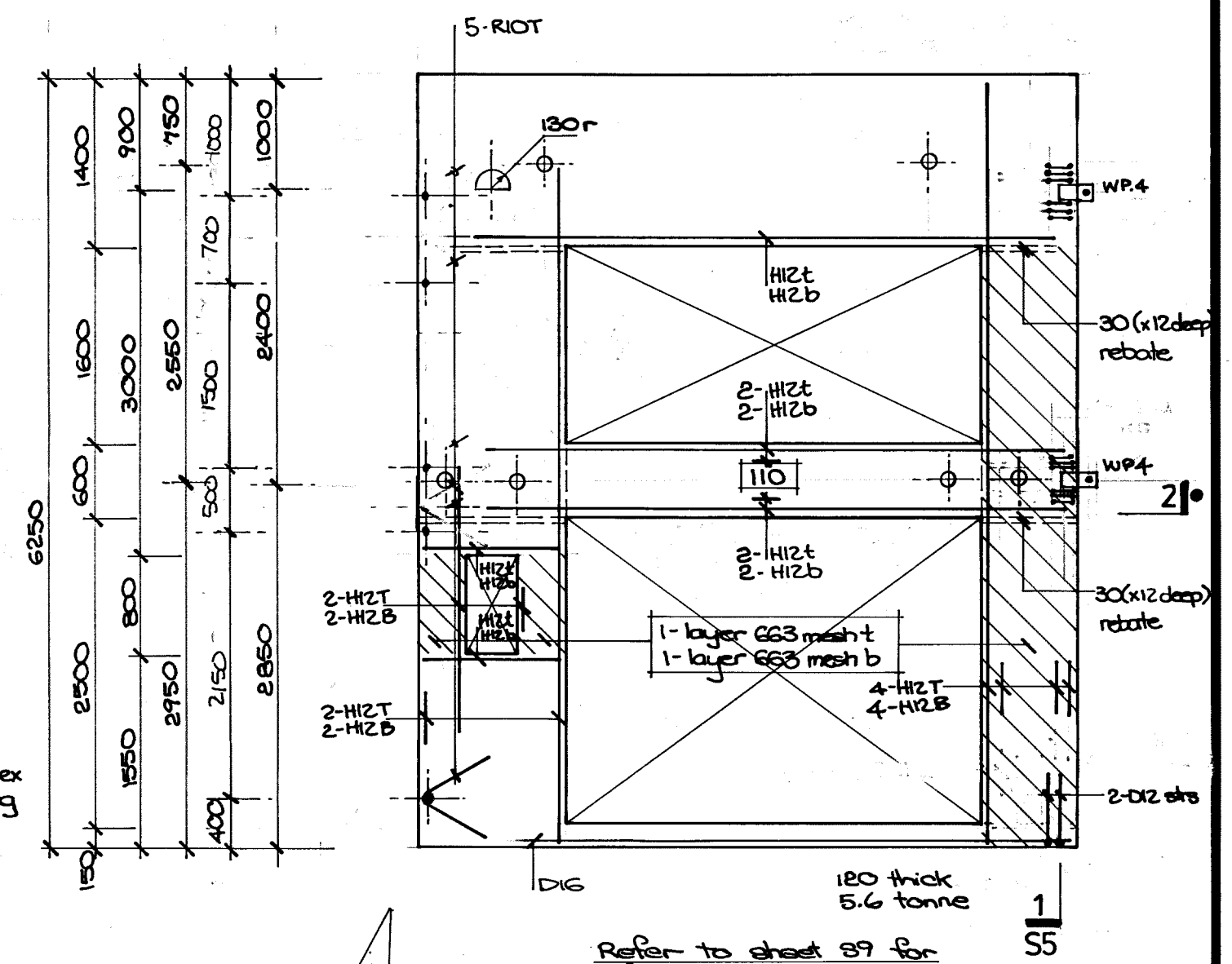
Refer to Panel M on sheet S8 for panel dimensions, lifting eyes, and reinforcing except where noted otherwise on this drawing.



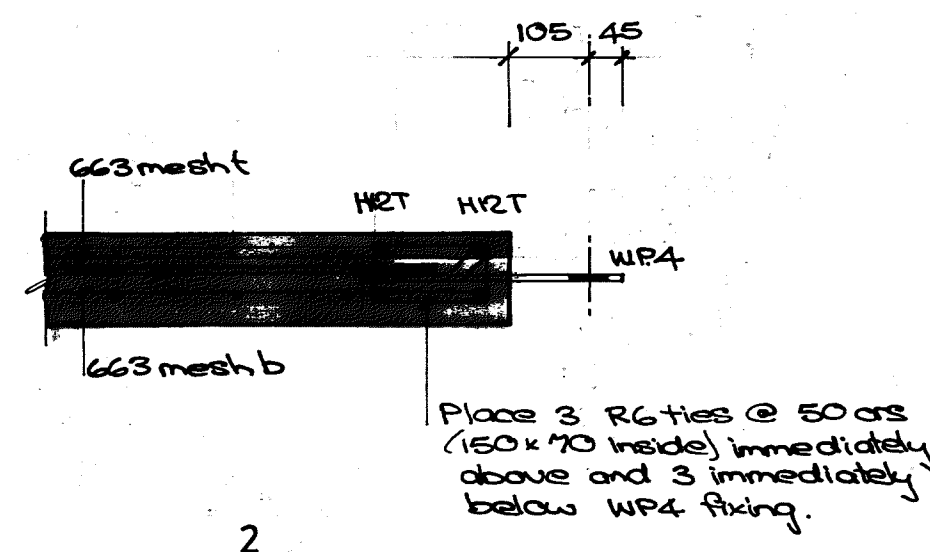
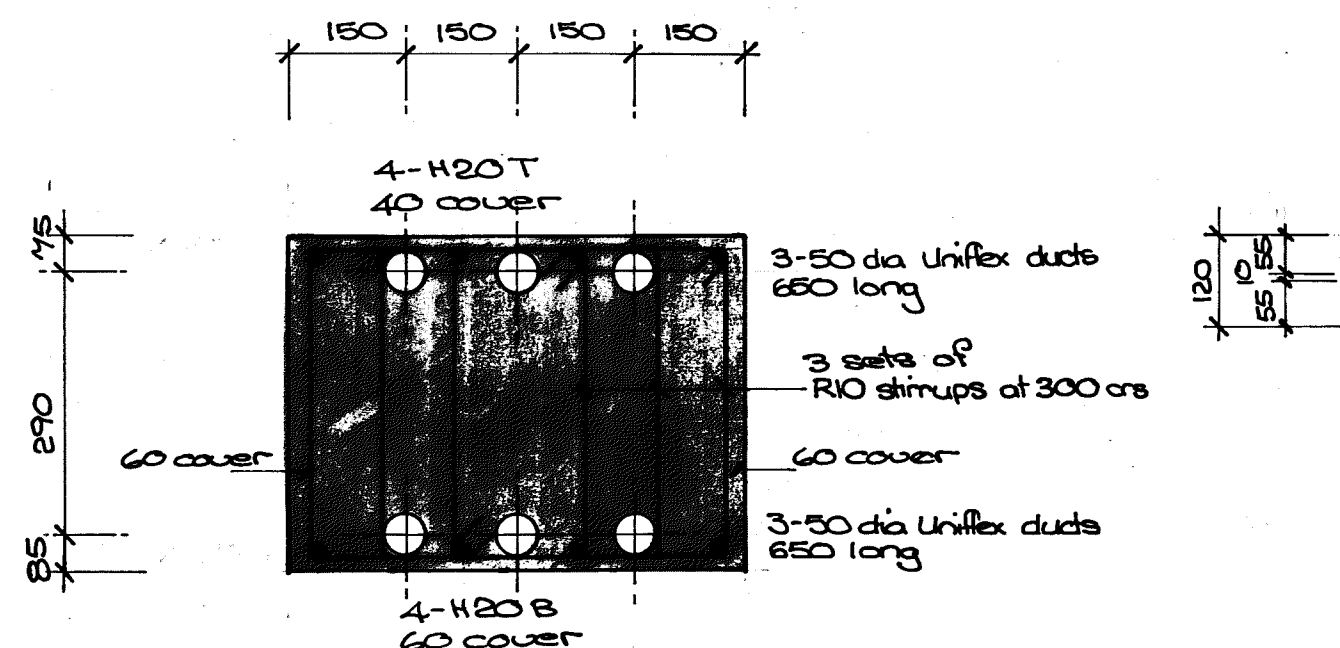
PANEL 23



PANEL 24



PANEL 25

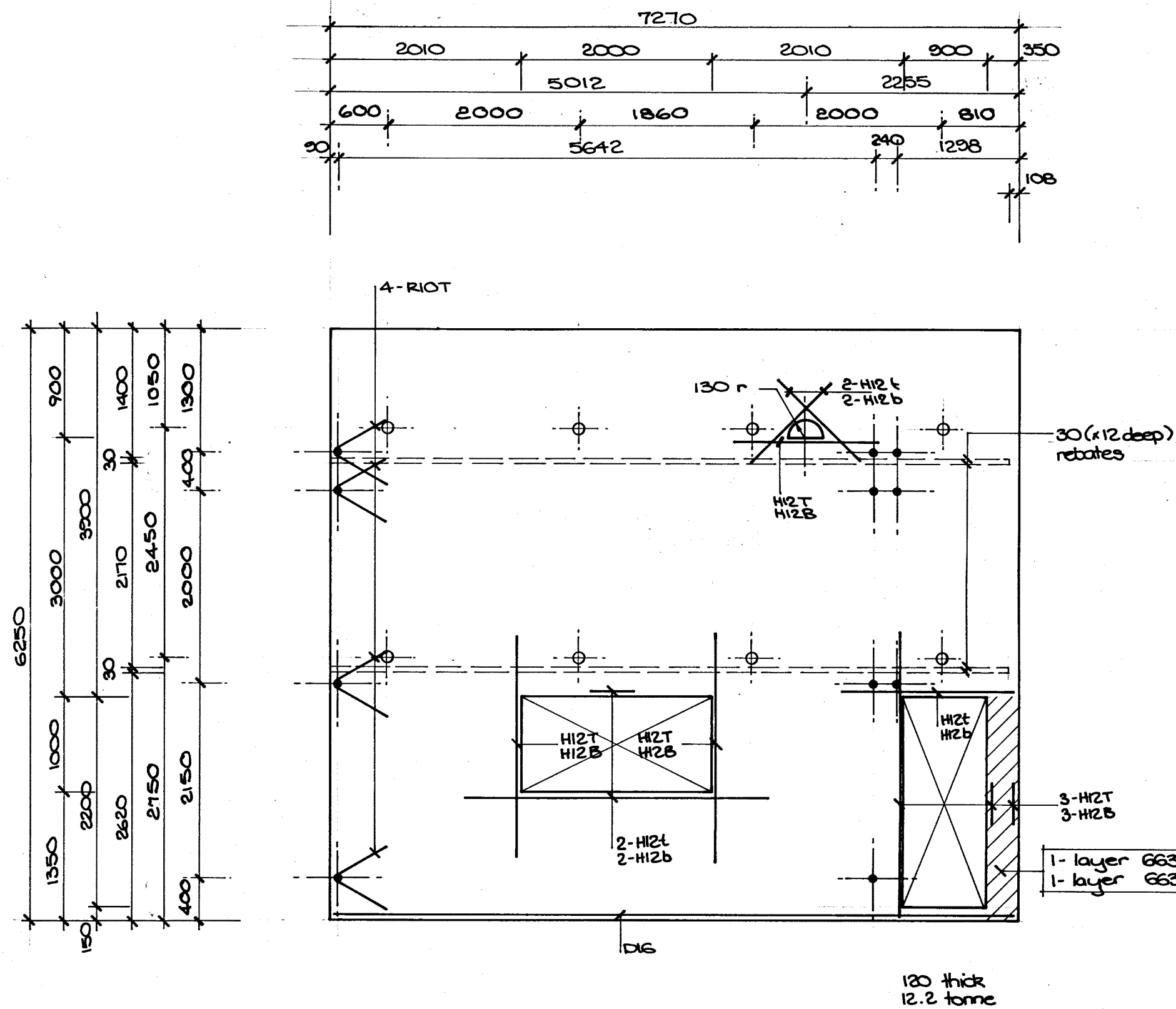


Refer to sheet S3 for notes

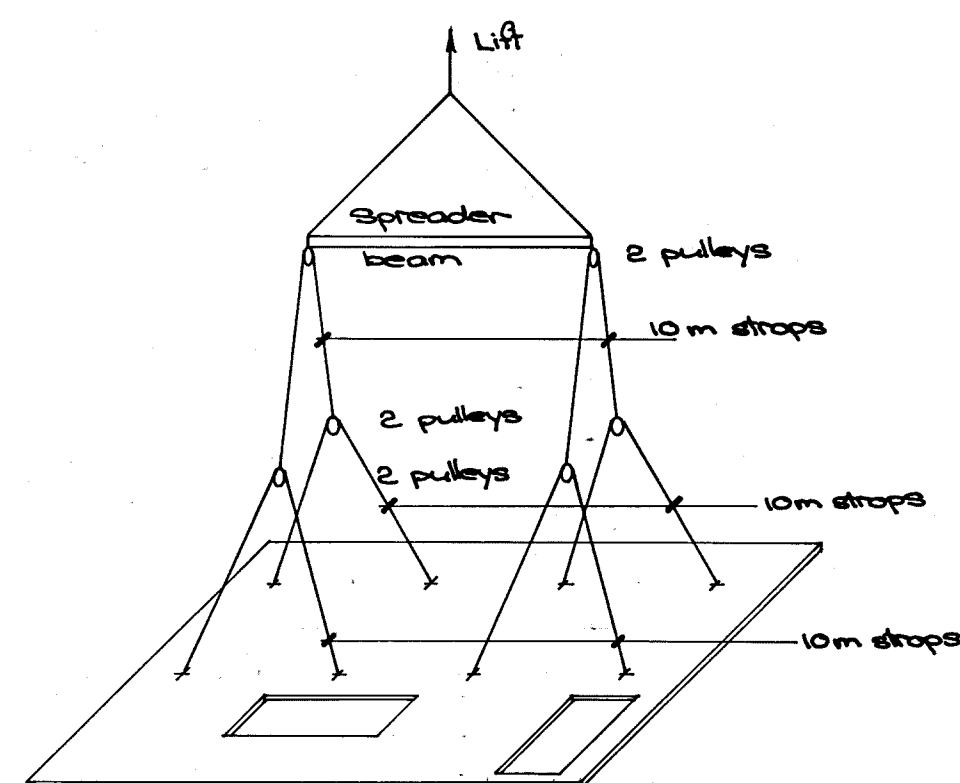
DEVELOPMENT — 121 — 123 BLENHEIM ROAD CHRISTCHURCH

DRN	CRC	APPROVED	DATE	SCALES	SHEET	FILE
DES			JUNE 1993	1:50	S11c	4860
CKD						

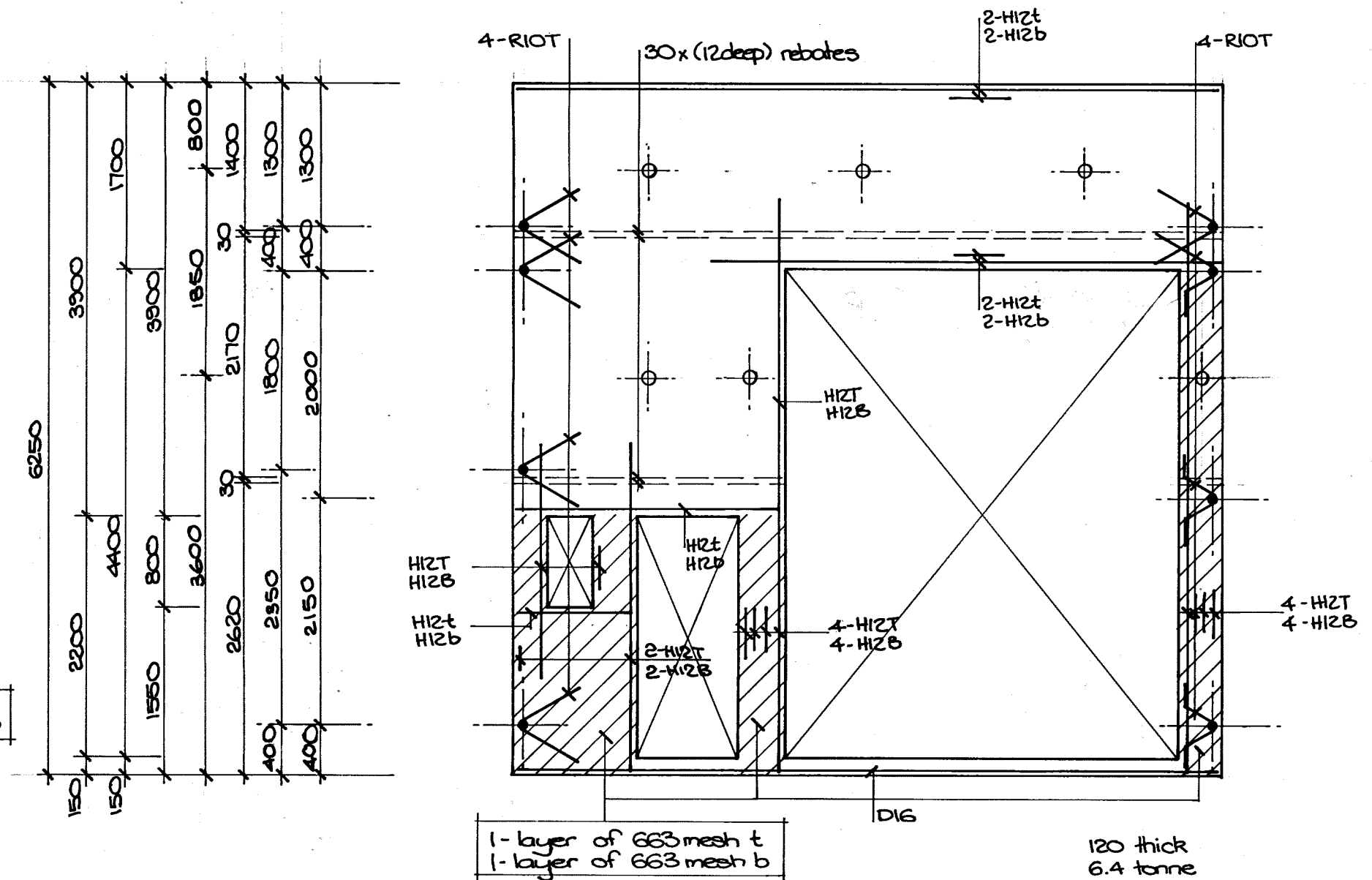
A 23-7-93 Changed DR-400 starters to D10 @ 275
 B 23-8-93 TAM FIXINGS ALTERED TO P25 & P24.
 C 30-8-93 TAM FIXINGS ALTERED TO P24.



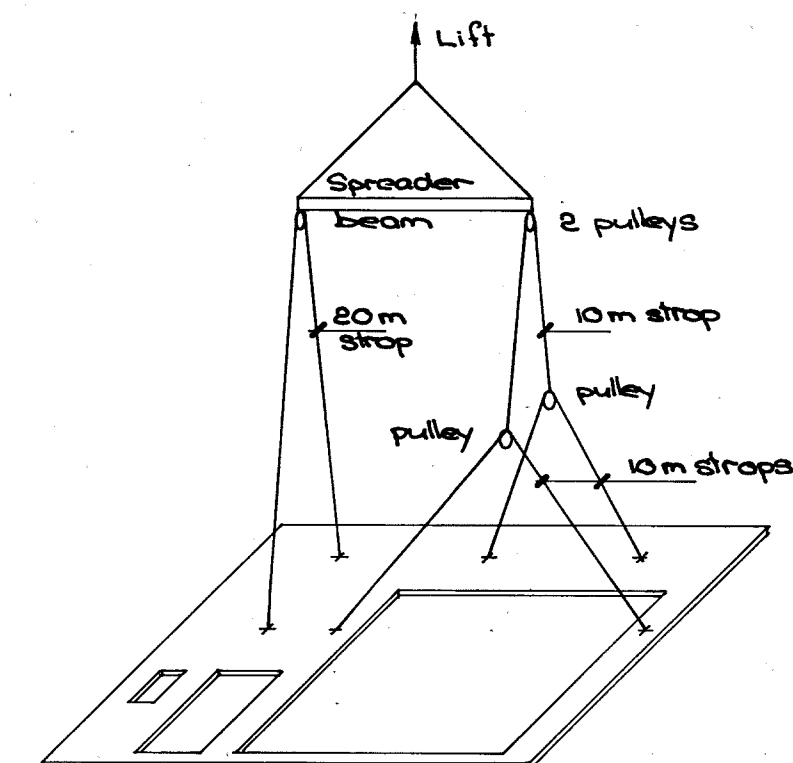
PANEL 26



LIFTING DIAGRAM - PANELS 26, 33, & 36

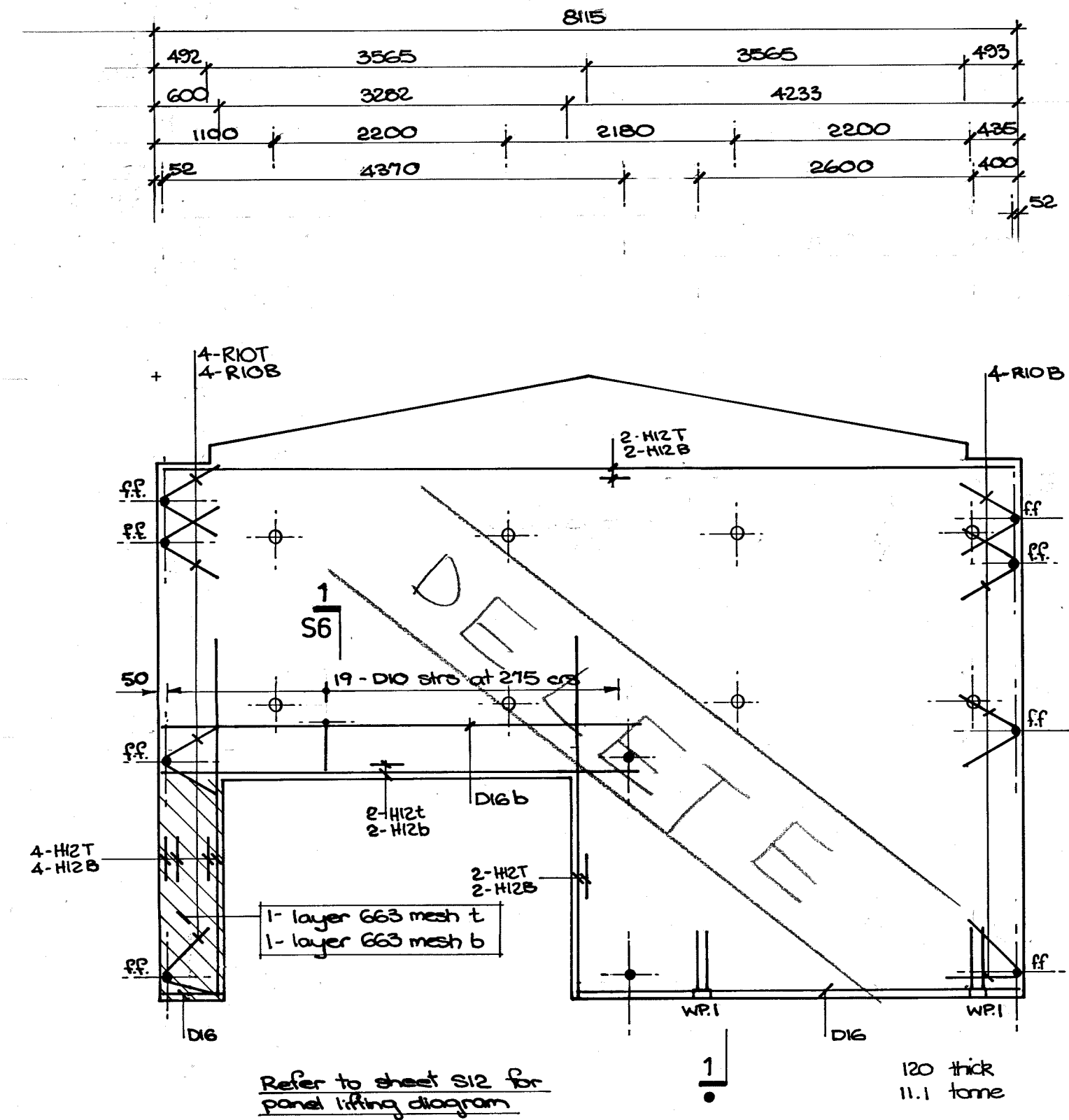
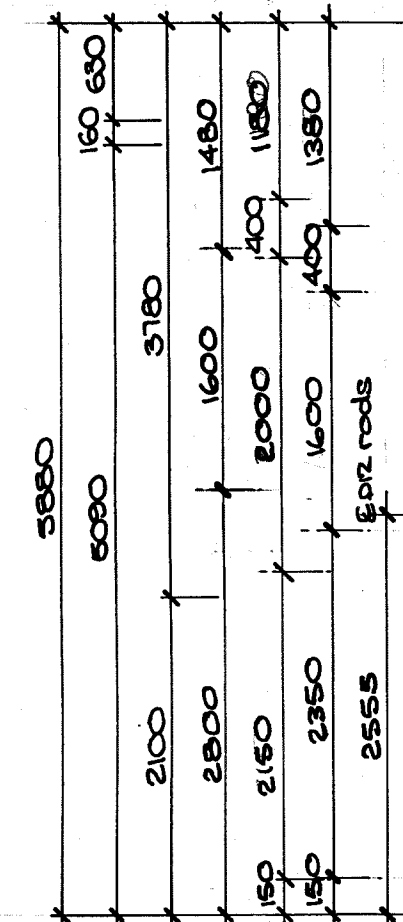


PANEL 27

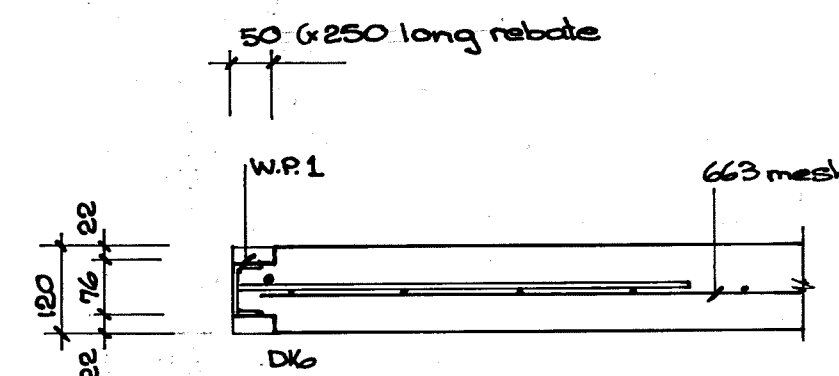


LIFTING DIAGRAM - PANEL 27

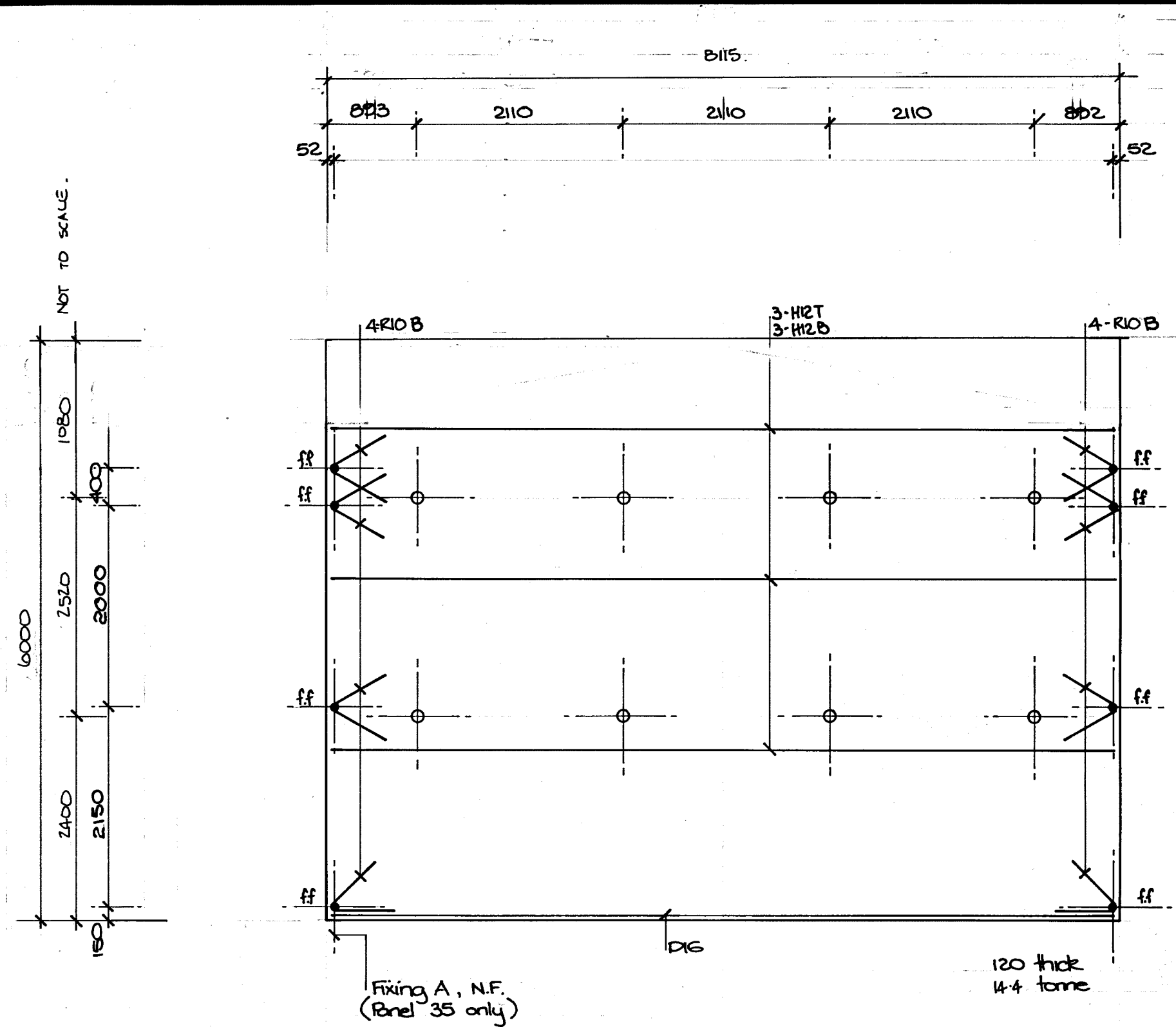
Refer to sheet S3 for notes



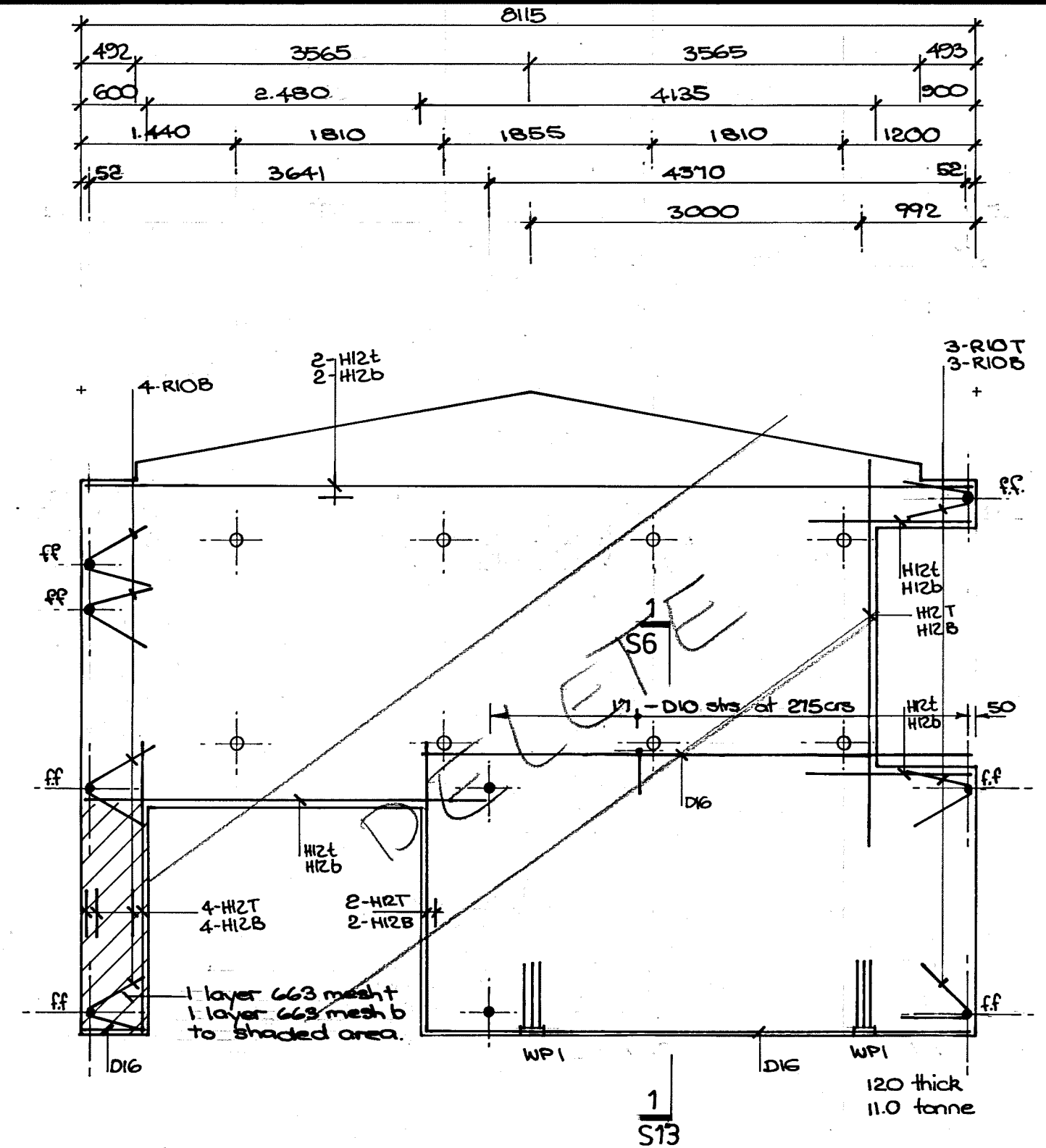
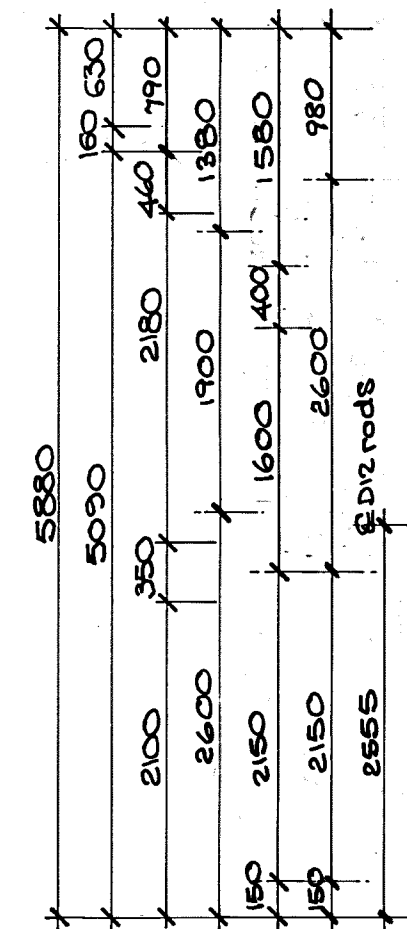
PANEL 33



Refer to sheet S3 for notes



PANELS 34 & 35



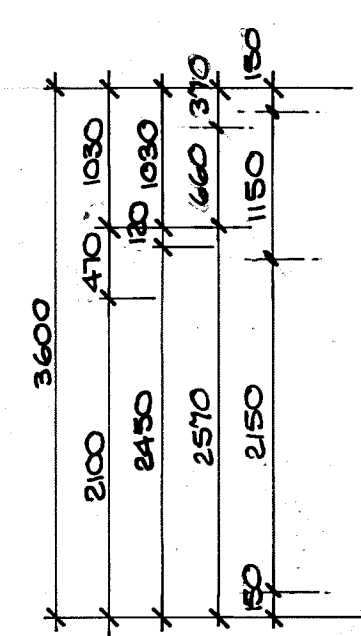
PANEL 36

Refer to sheet S3 for notes

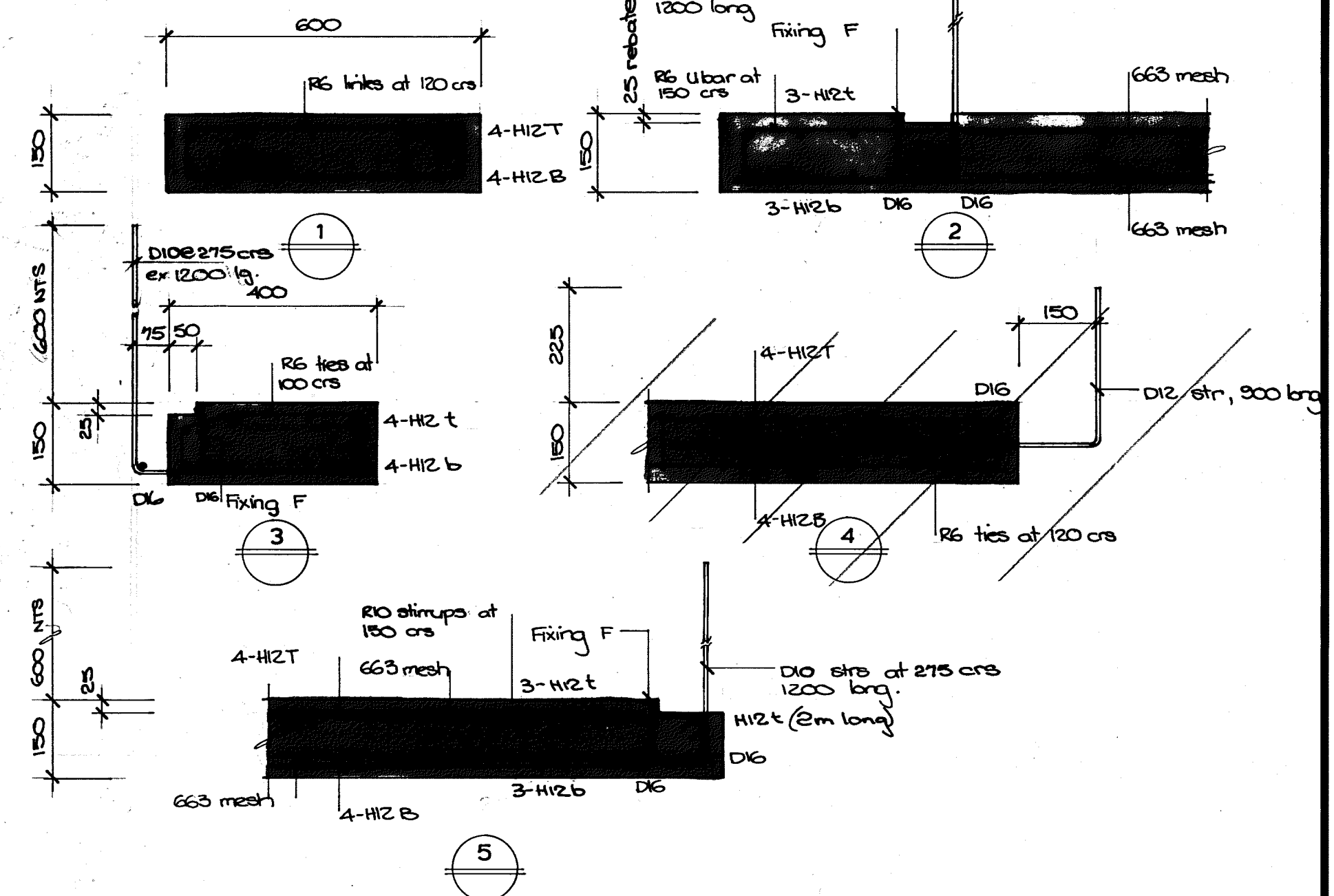
DEVELOPMENT — 121 — 123 BLENHEIM ROAD CHRISTCHURCH

DRN	C.P.C.	APPROVED	DATE	SCALES	PRECAST CONCRETE PANELS 34 — 36	SHEET	FILE
DES			JUNE 1993	1:50		S14	4860
CKD							

A 23-7-93 changed D12-400 starters to D10 @ 275
B 30-8-93 PANELS 34, 35 ALTERED, PANEL 36 DELETED.



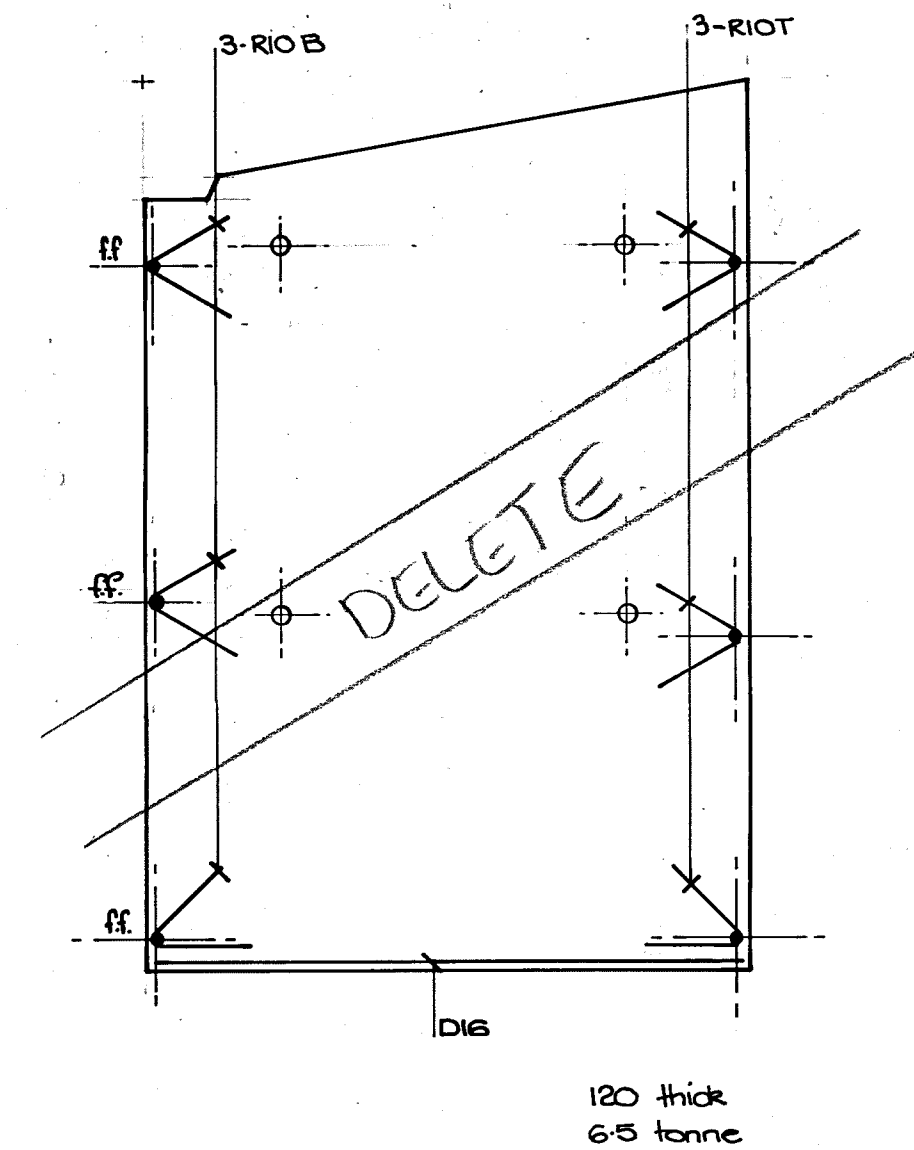
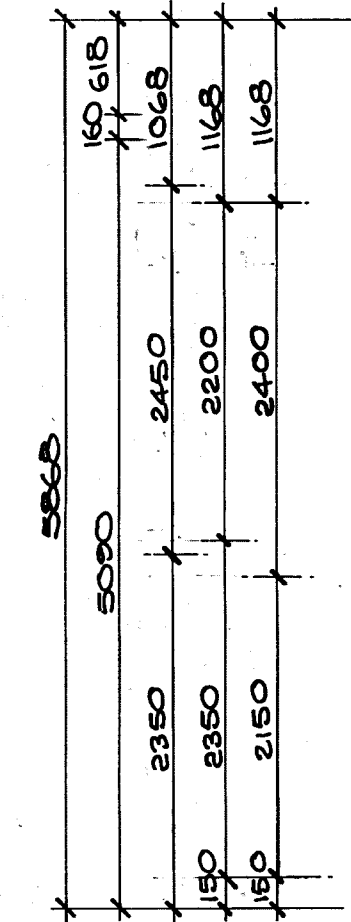
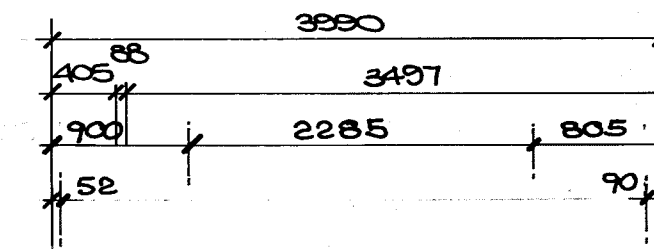
LIFTING DIAGRAM - PANEL 39



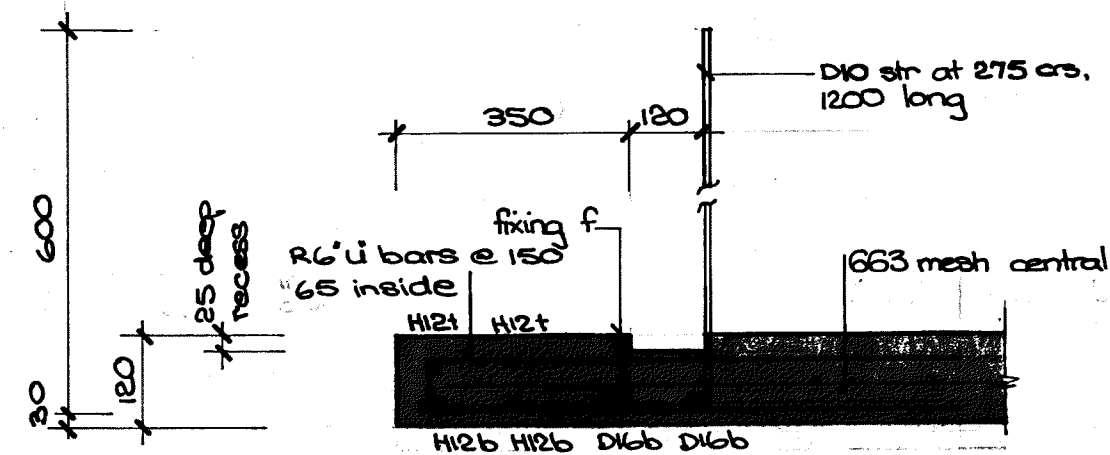
Refer to sheet S for notes

DRN	CPG	APPROVED	DATE	SCALES	PRECAST CONCRETE PANELS 37 - 39	SHEET	FILE
DES			JUNE 1993	1:50		S15A	4860
CKD							

A 23-7-93 changed D12-400 starters to D10 @ 215



PANEL 42



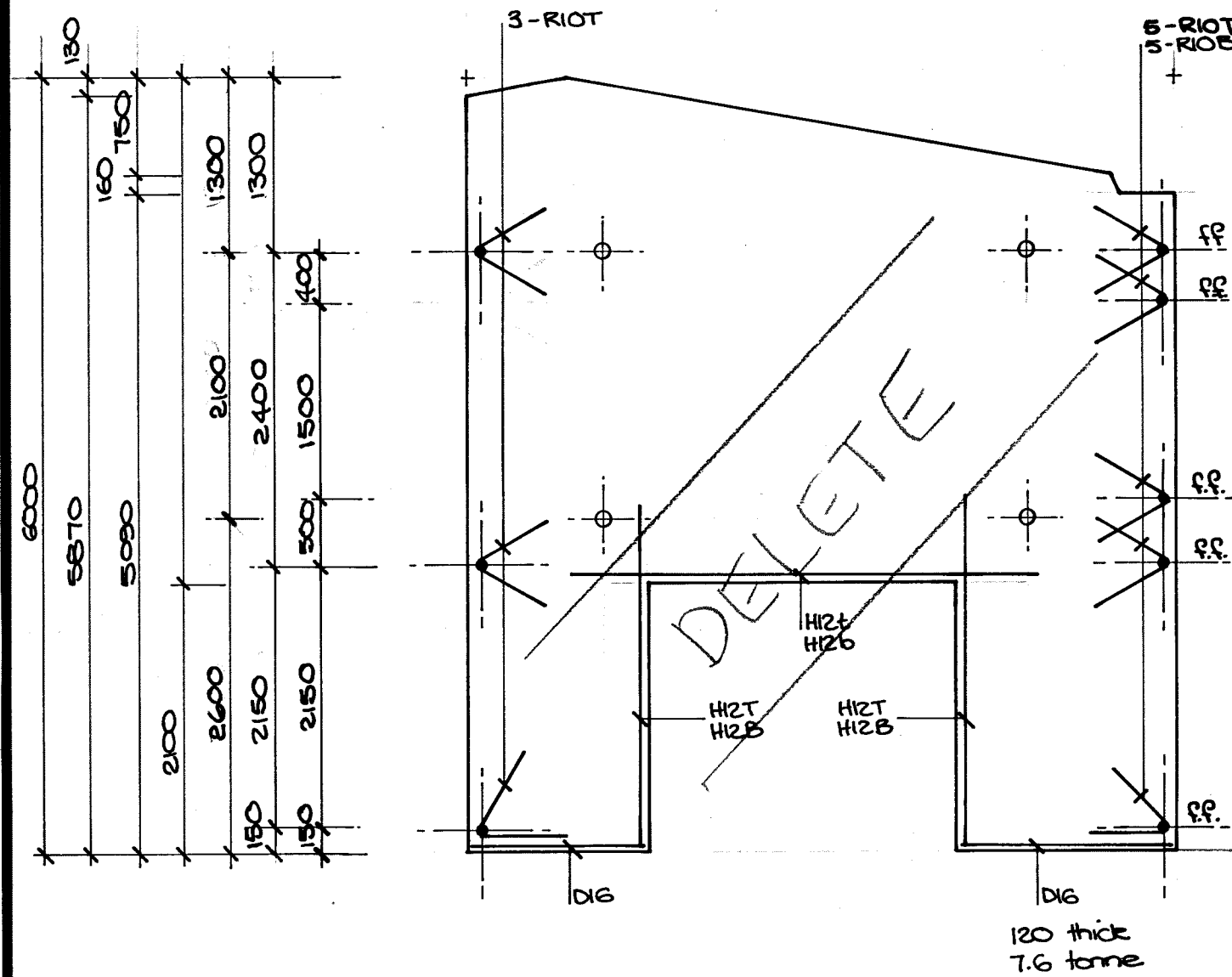
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Refer to sheet S3 for notes

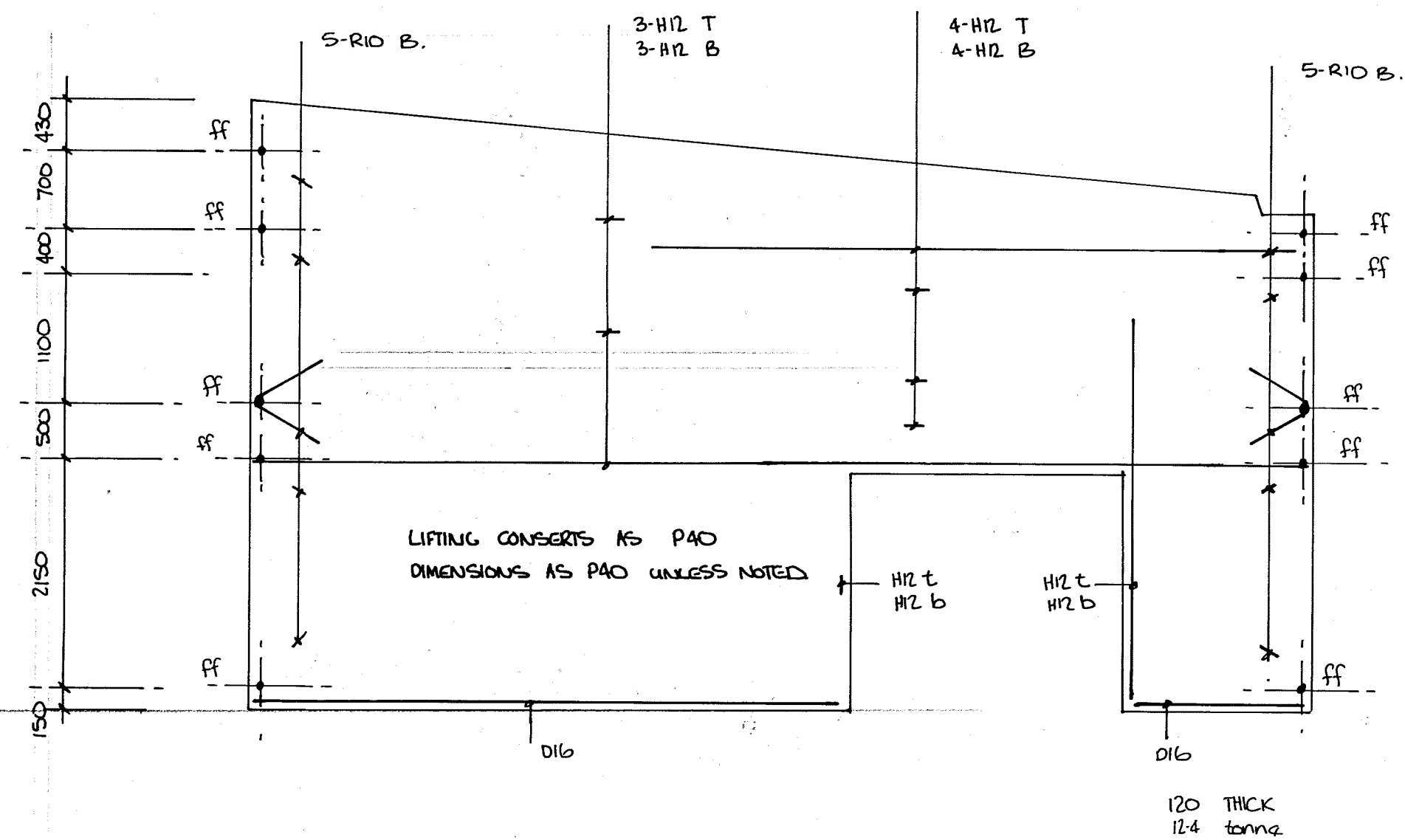
DRN	CRC	APPROVED	DATE	SCALES	PRECAST CONCRETE PANELS 40 & 42	SHEET	FILE
DES			JUNE 1993	1:50		S16 _A	4860
CKD							

A 23-7-93 changed D12-400 starters to D10 @ 275 cms
B 23-8-93 PANEL 40 ALTERED, PANEL 42 DELETED

738	5480	88
1380	4250	1405
1050	2400	1700
90	3265	1165
	5338	62



PANEL 41



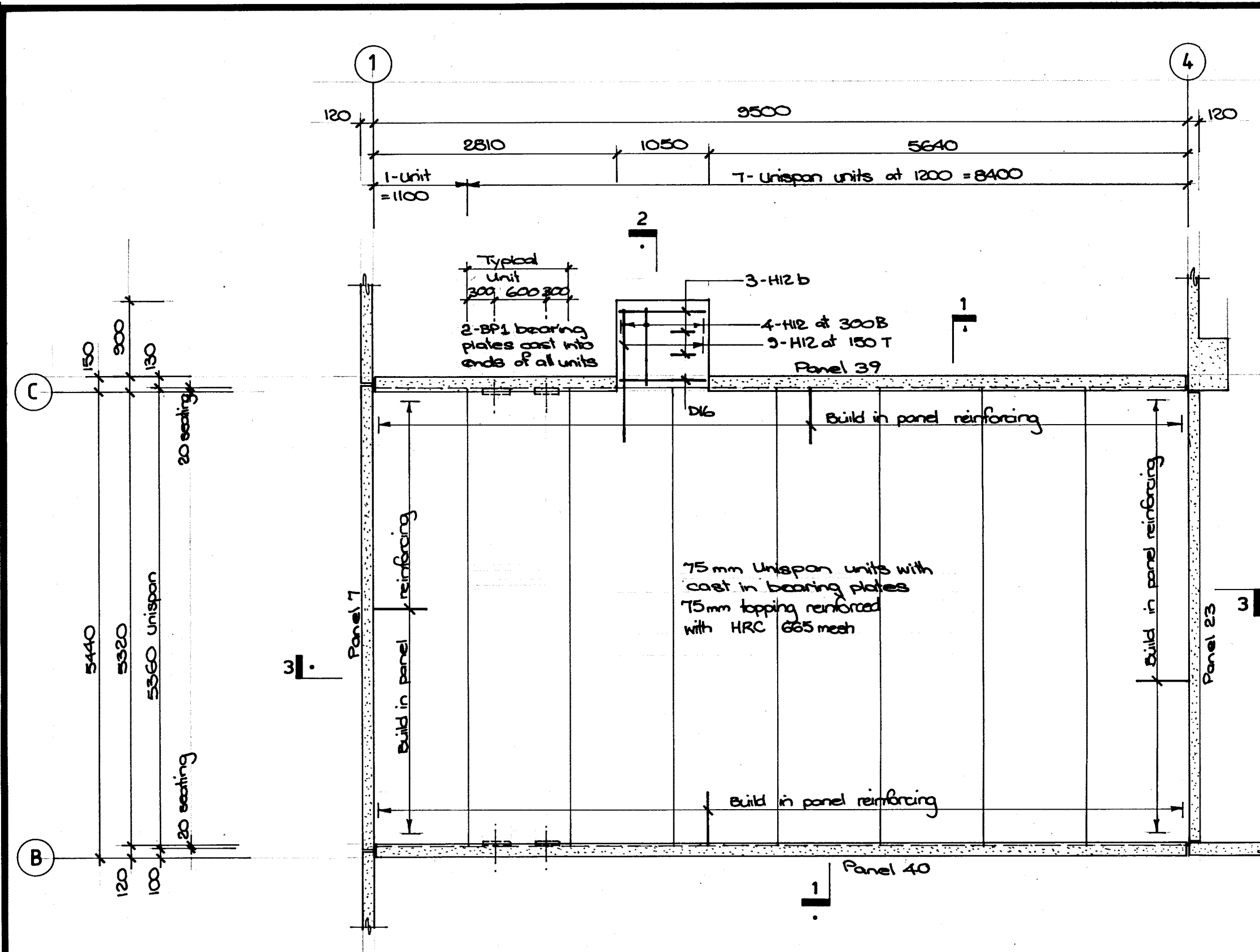
PANEL 41

Refer to sheet S3 for notes

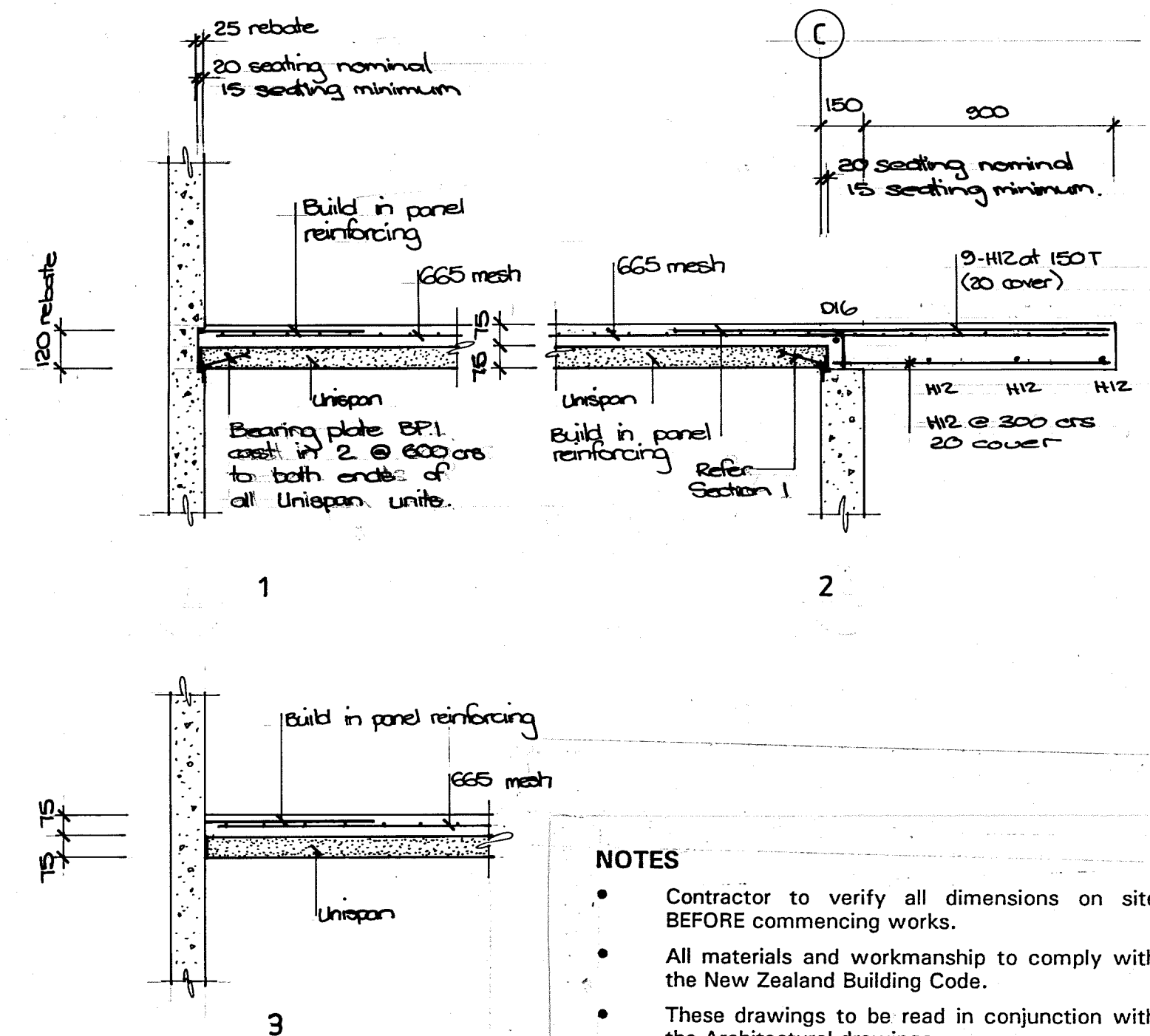
DEVELOPMENT - 121 - 123 BLENHEIM ROAD CHRISTCHURCH

DRN	DES	CKD	APPROVED	DATE	SCALES	PRECAST CONCRETE PANELS 41	SHEET	FILE
				JUNE 1993	1:50		S17A	4860

A 23-7-93 PANEL 41 REDRAWN

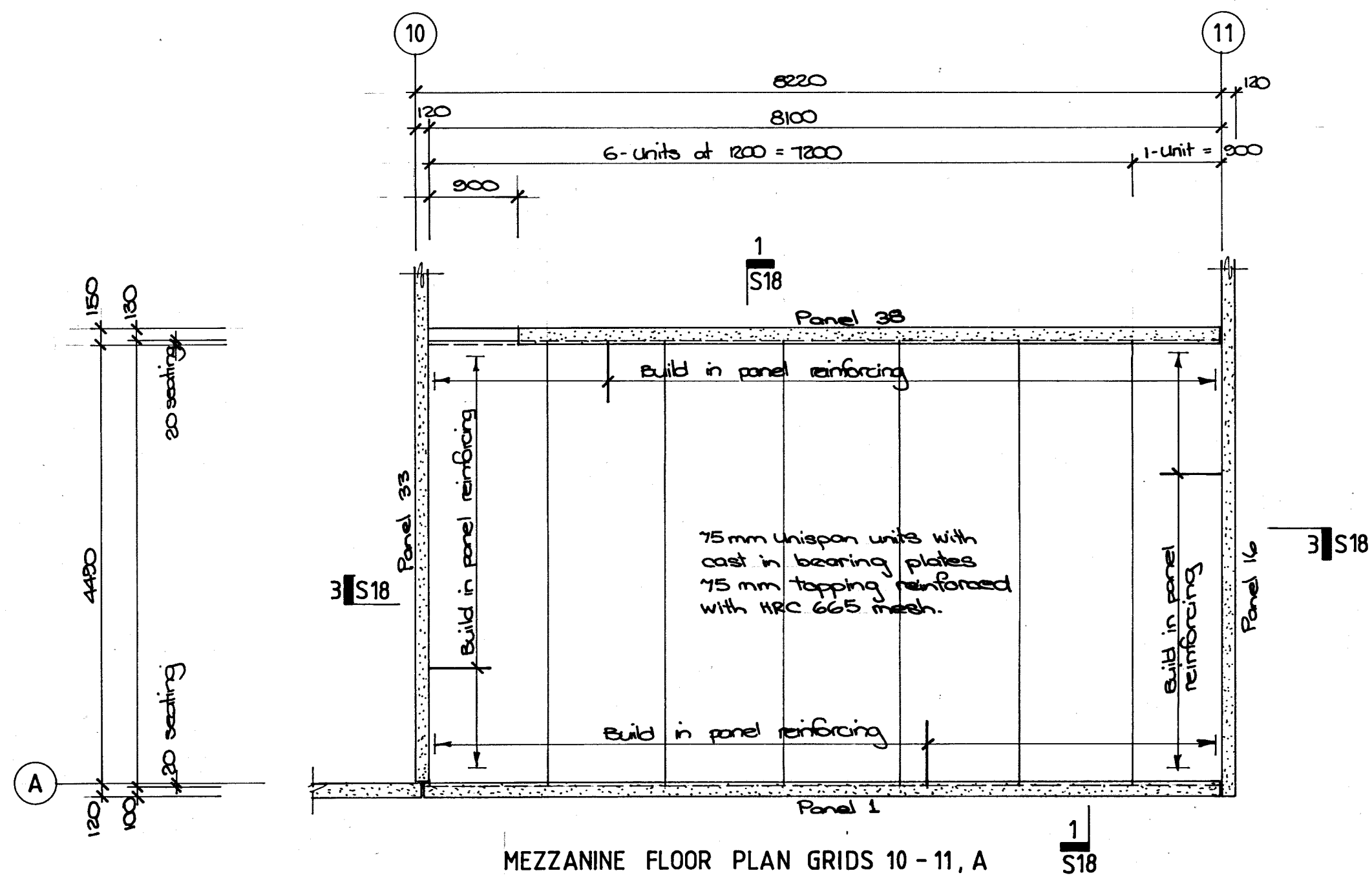
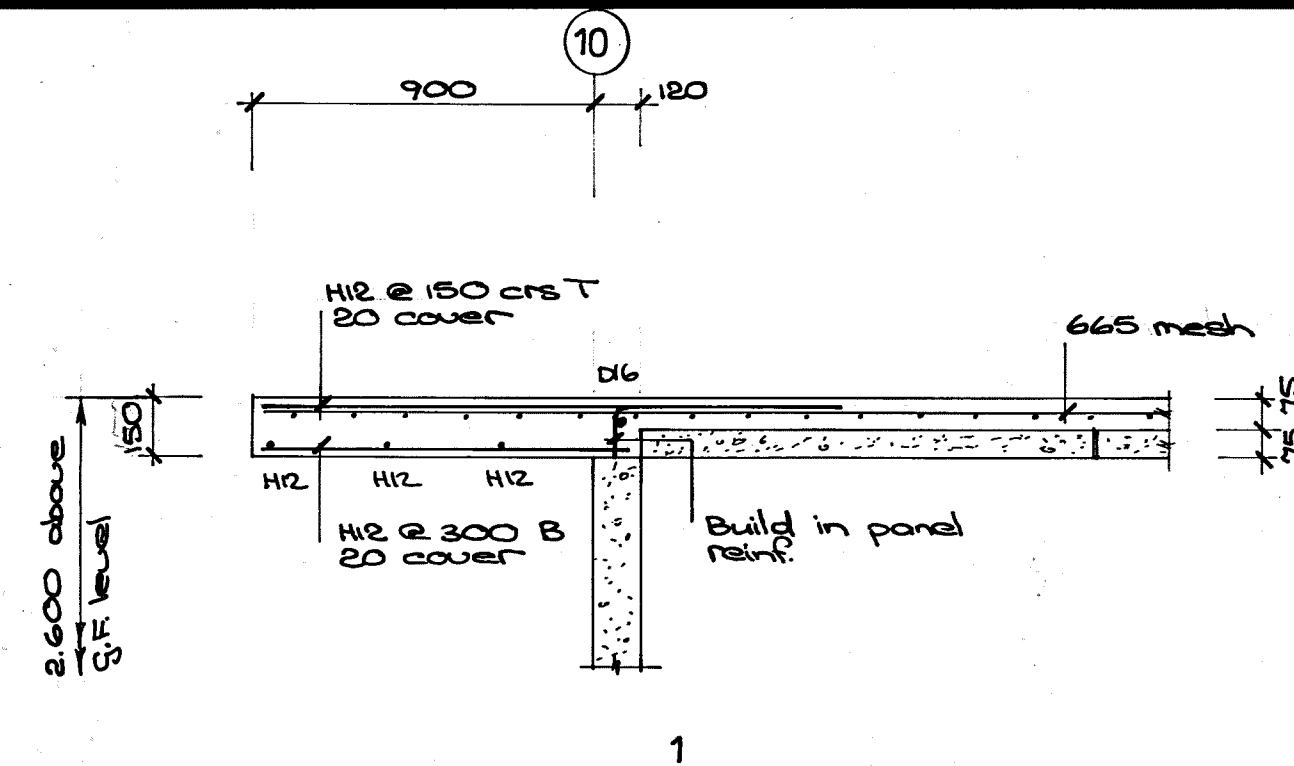
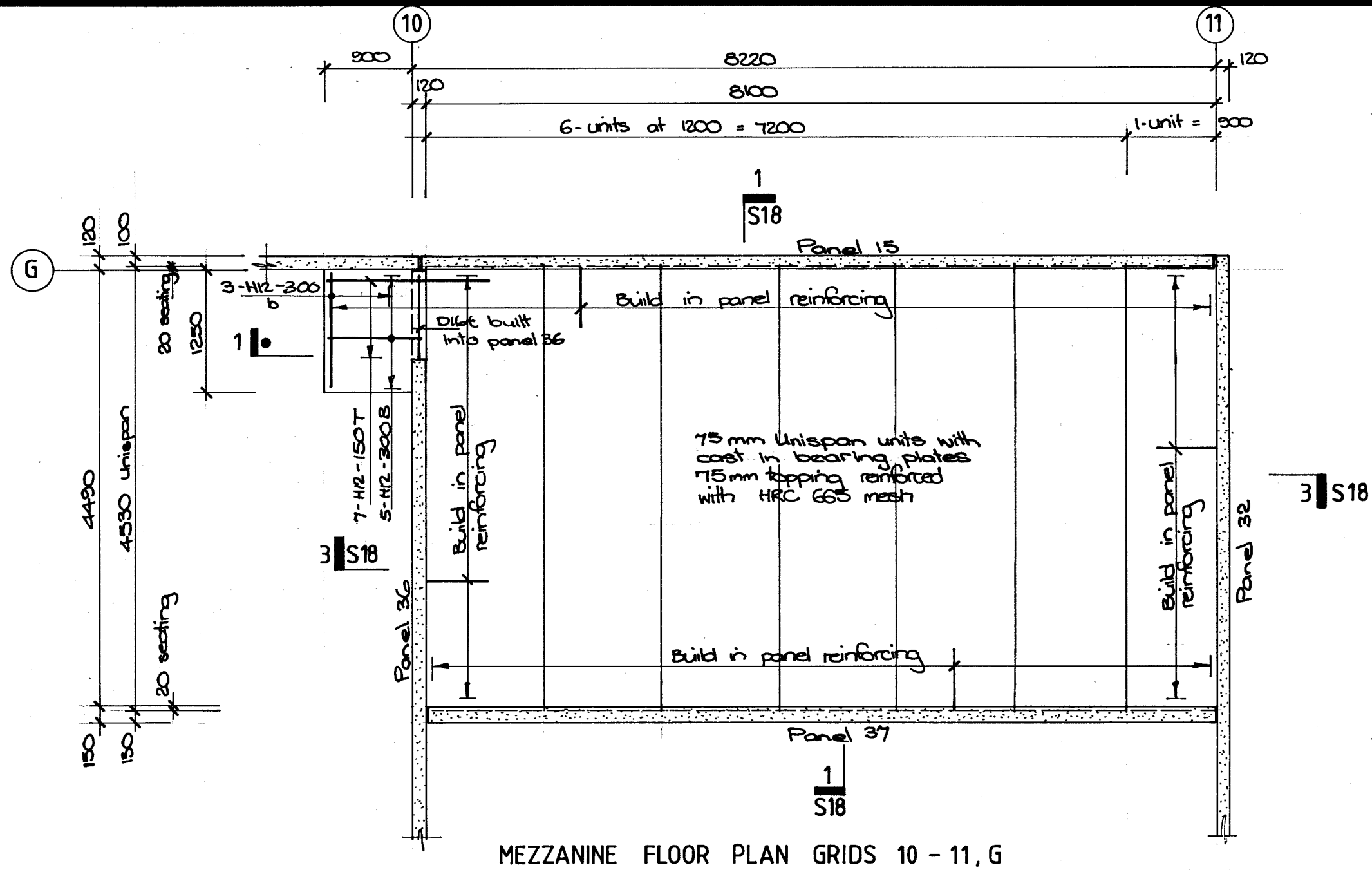


MEZZANINE FLOOR PLAN GRIDS B-C



NOTES

- Contractor to verify all dimensions on site BEFORE commencing works.
- All materials and workmanship to comply with the New Zealand Building Code.
- These drawings to be read in conjunction with the Architectural drawings.
- Refer Architects drawings for all nibs, holes, rebates etc.
- Use 75mm Unispan flooring system with 75mm min cast insitu topping where shown.
- Prestressed floor unit specification:-
 - All concrete construction is to be in accordance with the New Zealand Building Code.
 - Minimum concrete strength is to be 42 MPa at 28 days.
 - Use 5-10.9 dia stressing strands per 1.2m wide unit, load at transfer 72 kN/strand. Strand centre line 30, above soffit.
 - Prop at support and 1 row at mid point.
- Design parameters are as follows:
 - Loads : Live load 3.0 kPa
Superimposed dead load 0.5 kPa
 - Fire Rating : ½ hour
 - Deflection : Maximum precamber 5.0mm
Maximum long term deflection 5.0mm.
(less allowance for precamber)
- Where precast units are designed to be installed with a precamber, topping is to be cast with a matching precamber.
- Topping concrete strength is to be a minimum of 25 MPa at 28 days. The maximum slump is 100mm.
- Topping is to be reinforced throughout with 665 mesh. Lap all mesh a minimum of 2 cross wires, but no less than 225mm.
- All flooring systems to be propped in accordance with manufacturers specifications.



Refer to sheet S18 for notes

FRAMING PLAN

NOTES:

All materials & workmanship to comply with the N.Z. Building Code.

Contractor to verify all dimensions / on site before ordering / fabrication of steelwork.

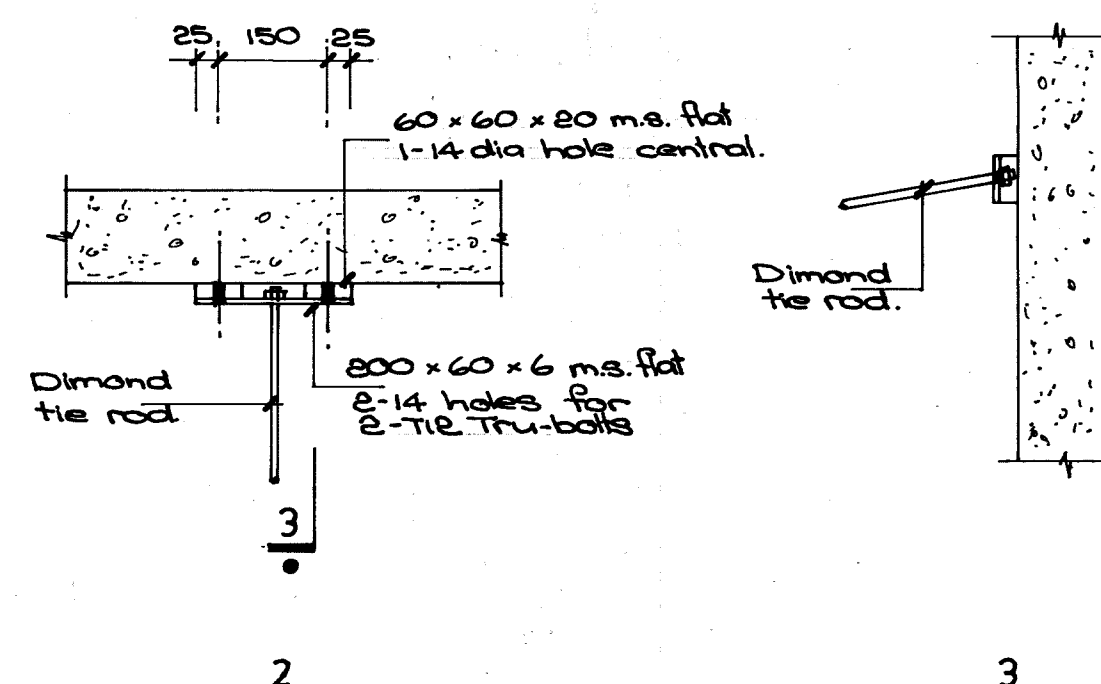
All purlins to be formed from galvanised 450 MPa steel.

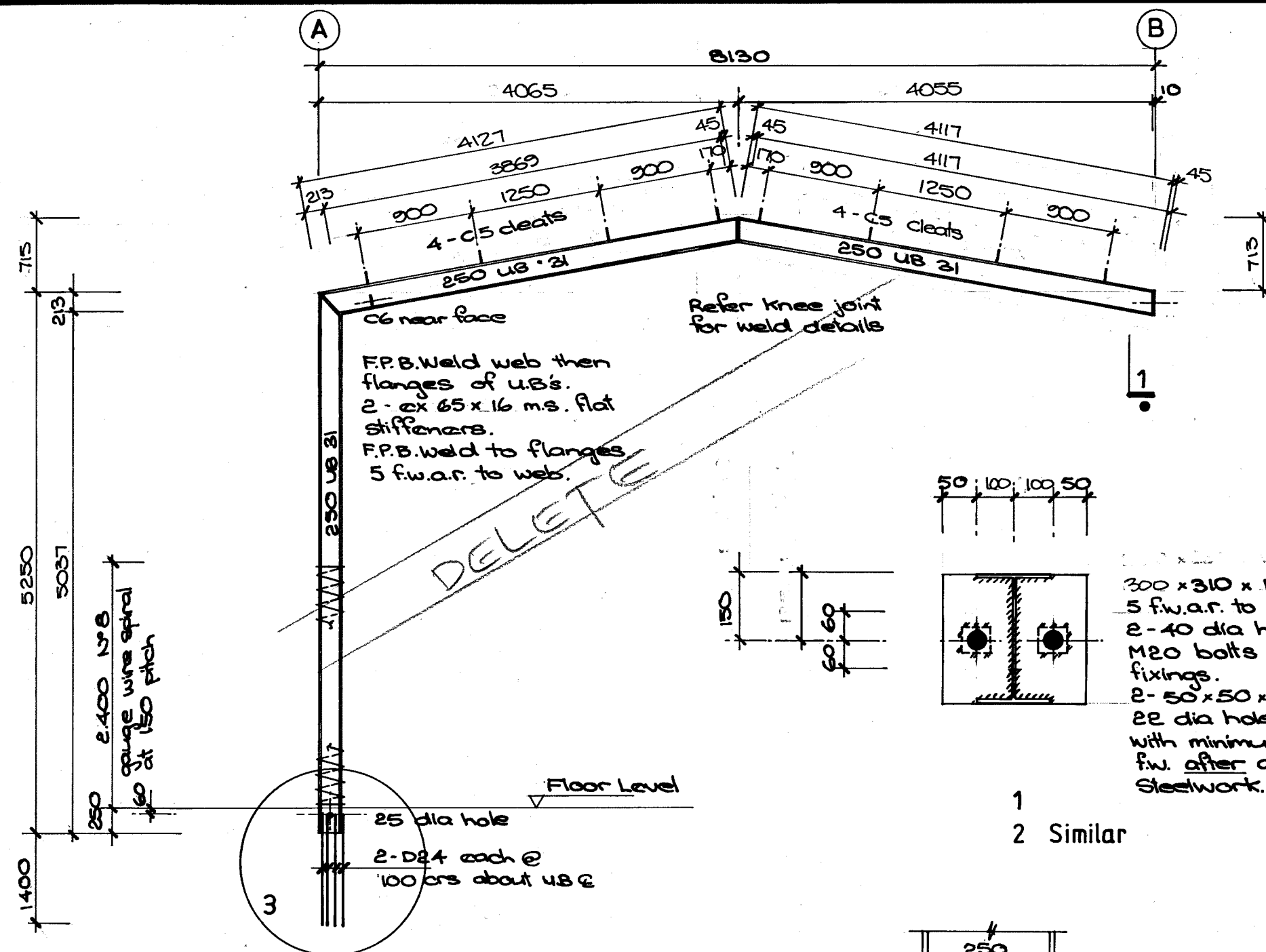
All holes in purlins to be 14 dia punched

PURLIN SIZES

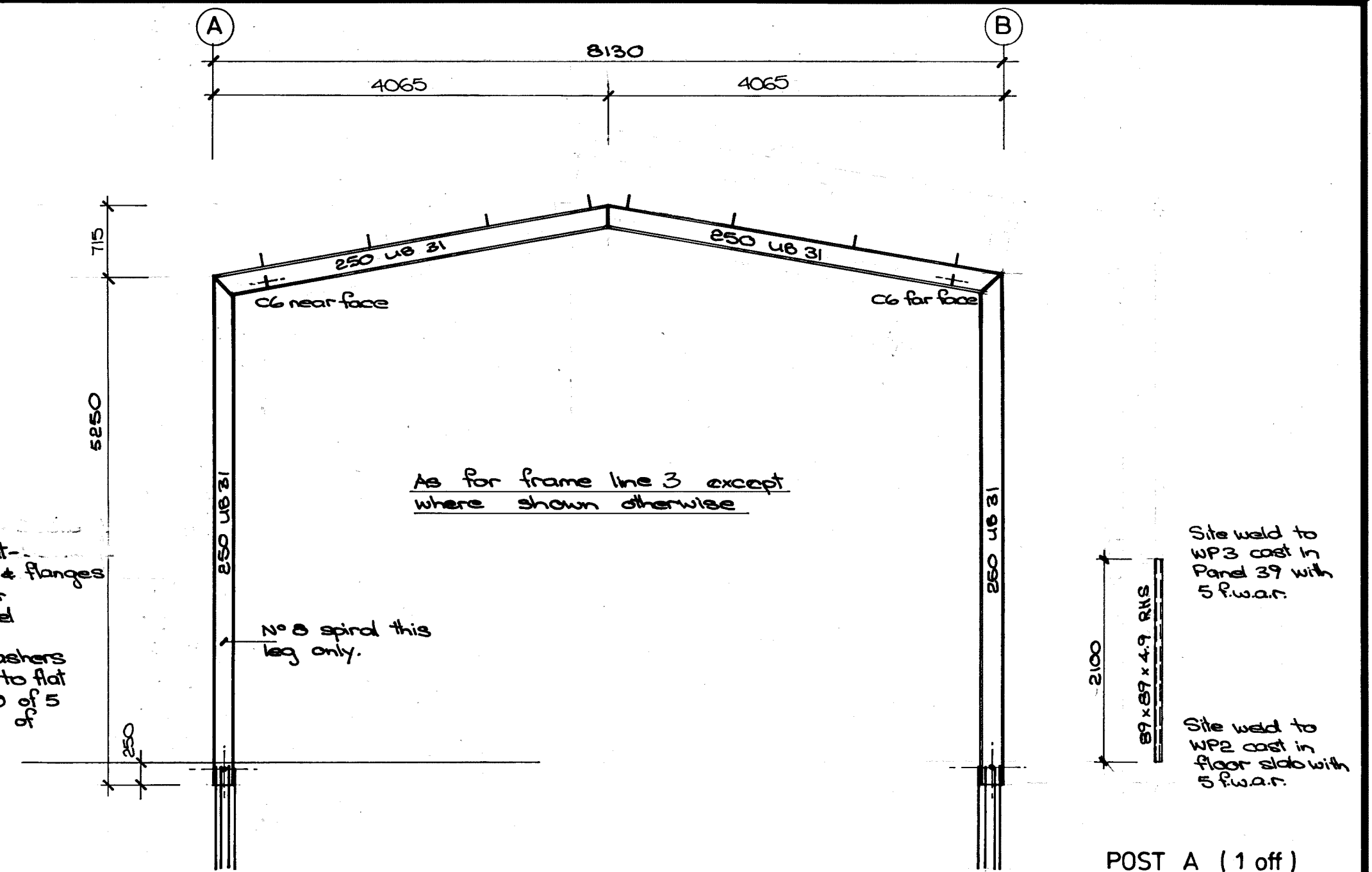
P2 - P5 BP 150/19
P1, P6 - P9 BP 200/25

All purlins braced with Fletcher Dimond galvanised brace channel & tie rod system.
(Tie rods only required where noted, units A & C.)

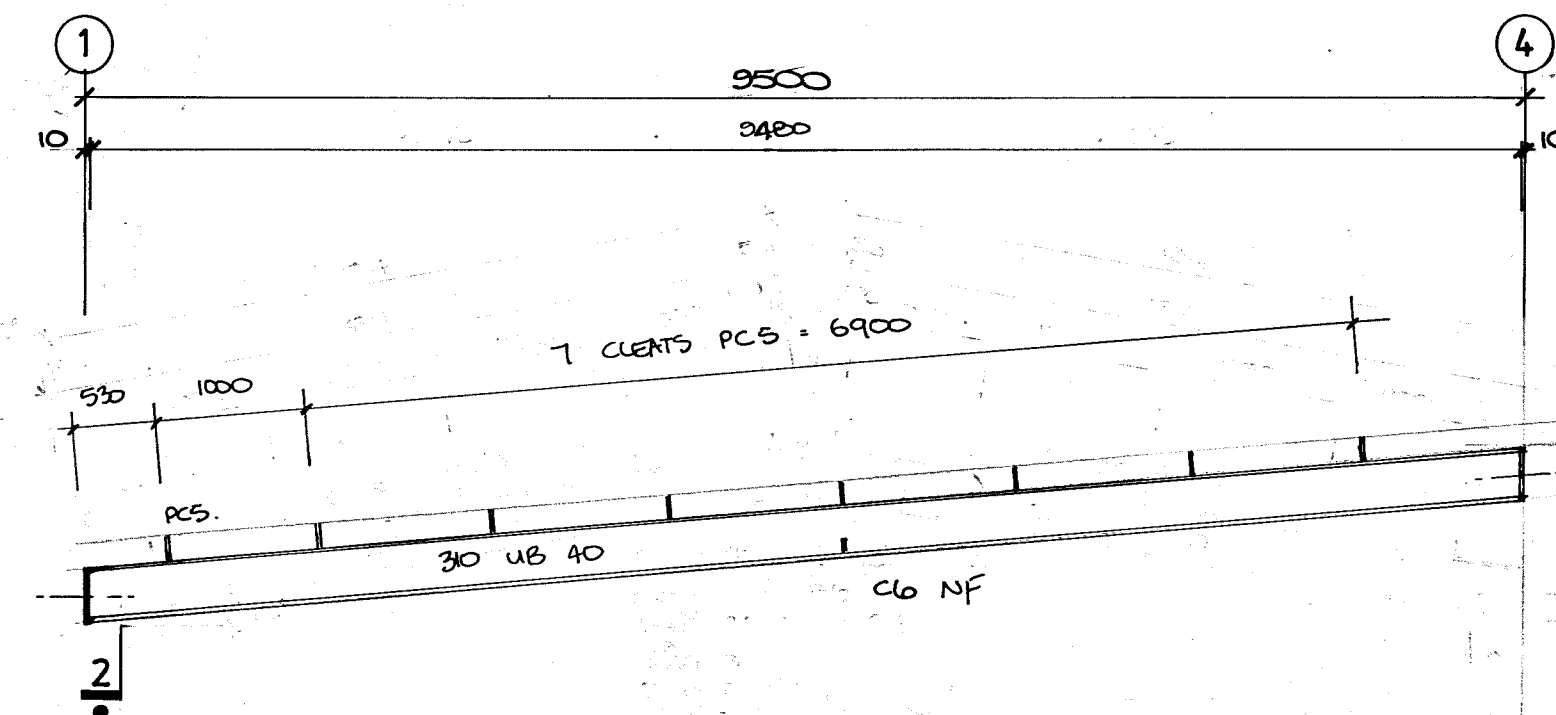




FRAME LINE 3



FRAME LINES 7, 8, & 9



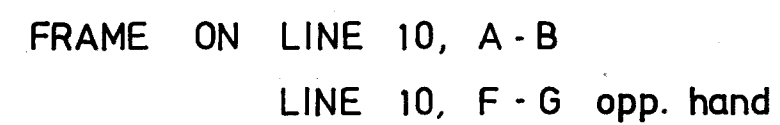
FRAME LINE D'

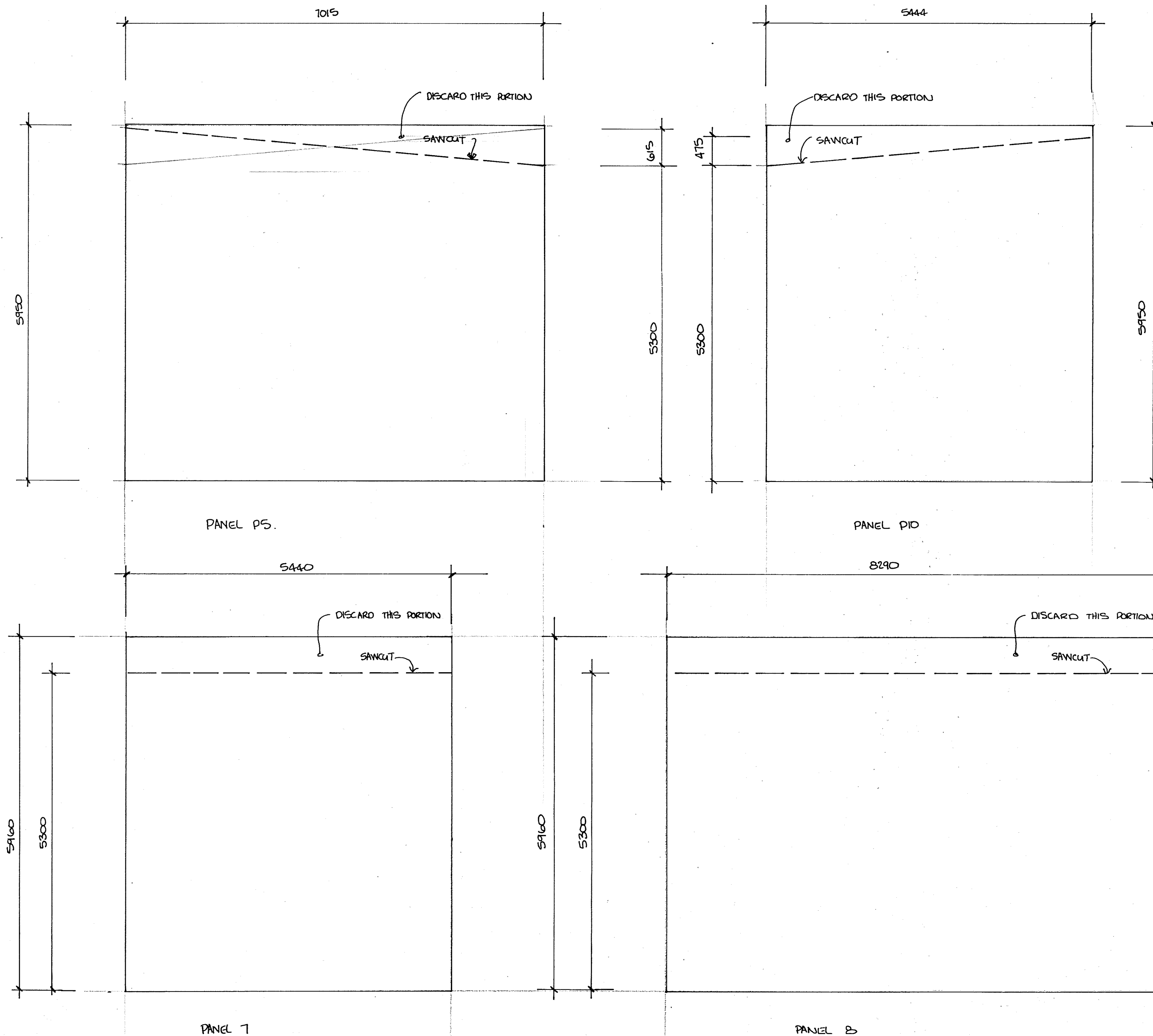
Refer to sheet S20 for notes

DEVELOPMENT - 121 - 123 BLENHEIM ROAD CHRISTCHURCH

DRN	W.L.S.	APPROVED	DATE	SCALES	SHEET	FILE
DES			JUNE 1993	1:50 1:10	STEELWORK FRAMES	S21
CKD						4860

A 30-8-93 FRAMES 2,3 DELETED, FRAME D' ALTERED

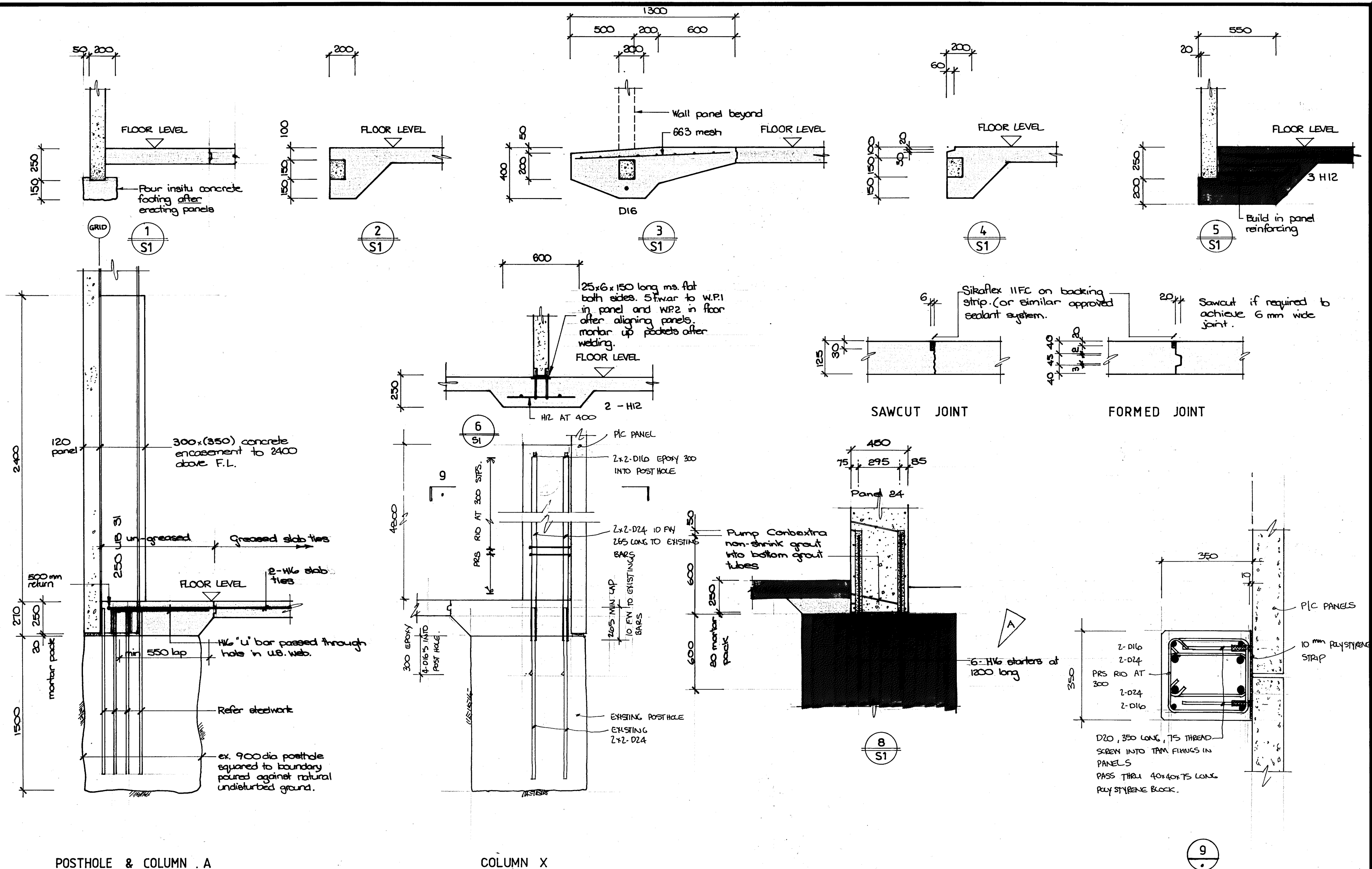




NOTE:
ALTERNATIVE LIFTING DEVICES
TO BE ADVISED BEFORE PANELS
LIFTED.

DEVELOPMENT - 121 - 123 BLENHEIM ROAD CHRISTCHURCH

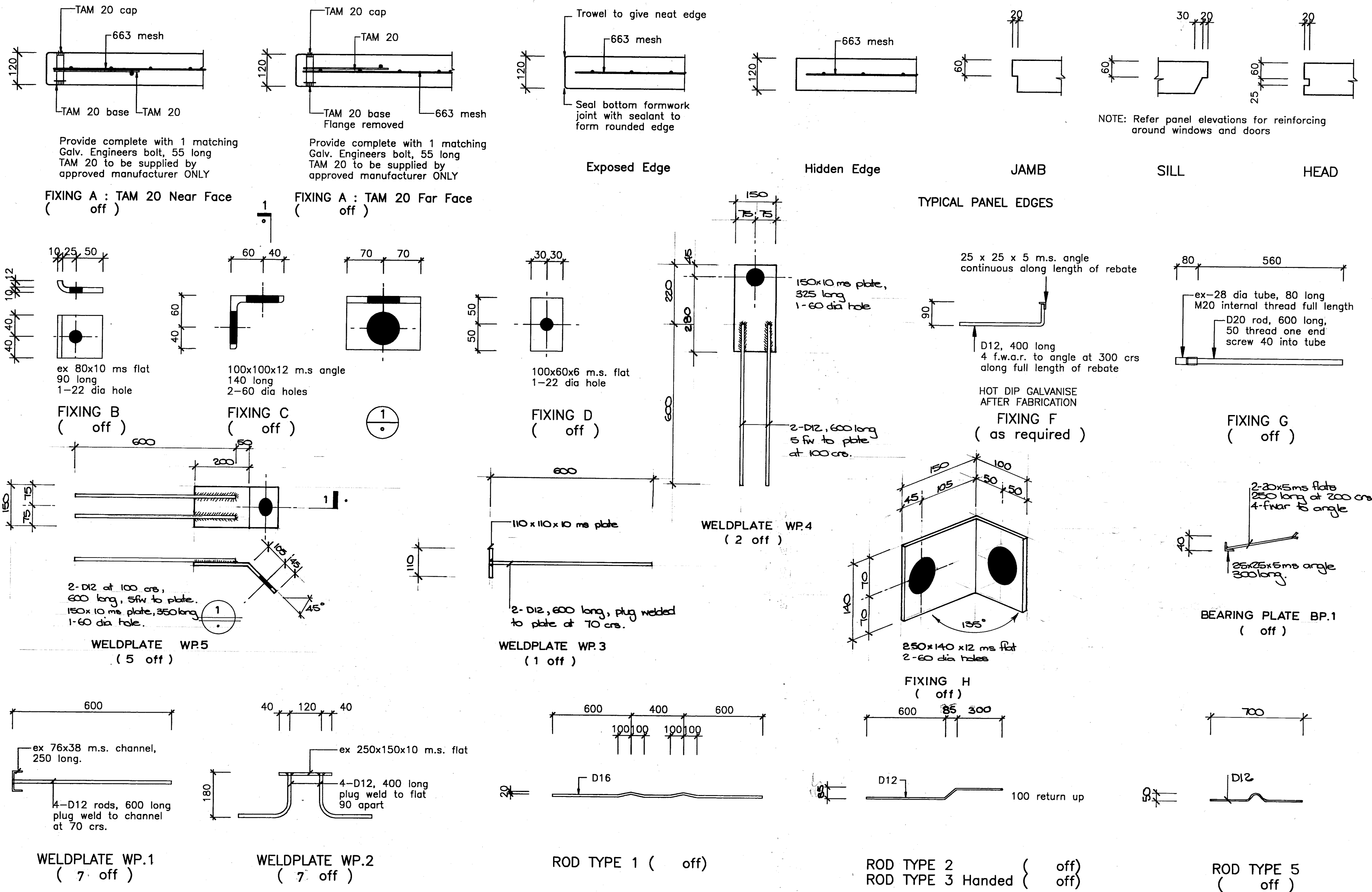
DRN		APPROVED	DATE	SCALES	SHEET	FILE
DES			19 AUG 1993	1:50	EXISTING PANELS CUT DOWN TO SUIT TRANS POWER REQUIREMENTS	
CKD					S23	4860

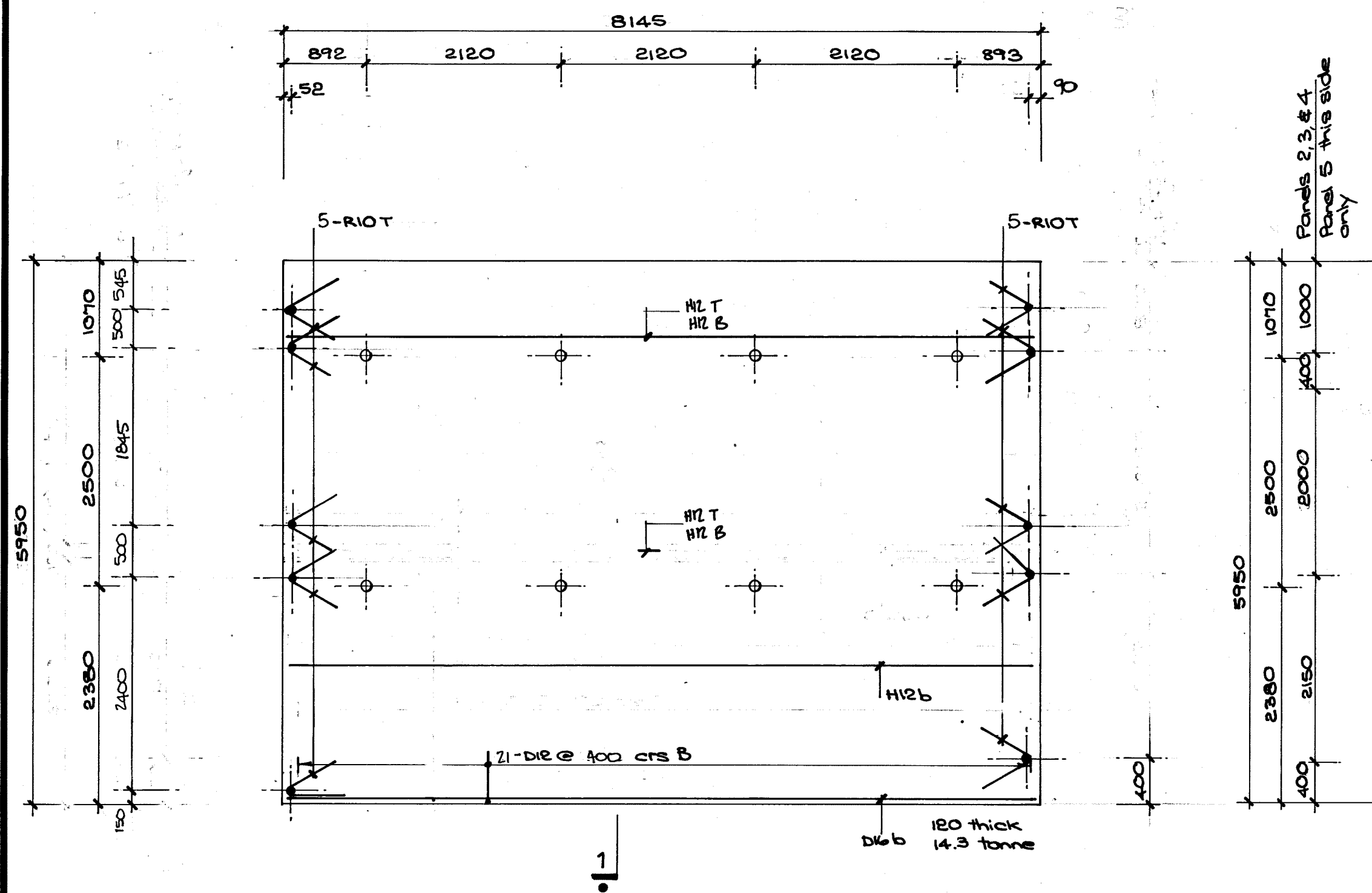


DEVELOPMENT — 121 — 123 BLENHEIM ROAD CHRISTCHURCH

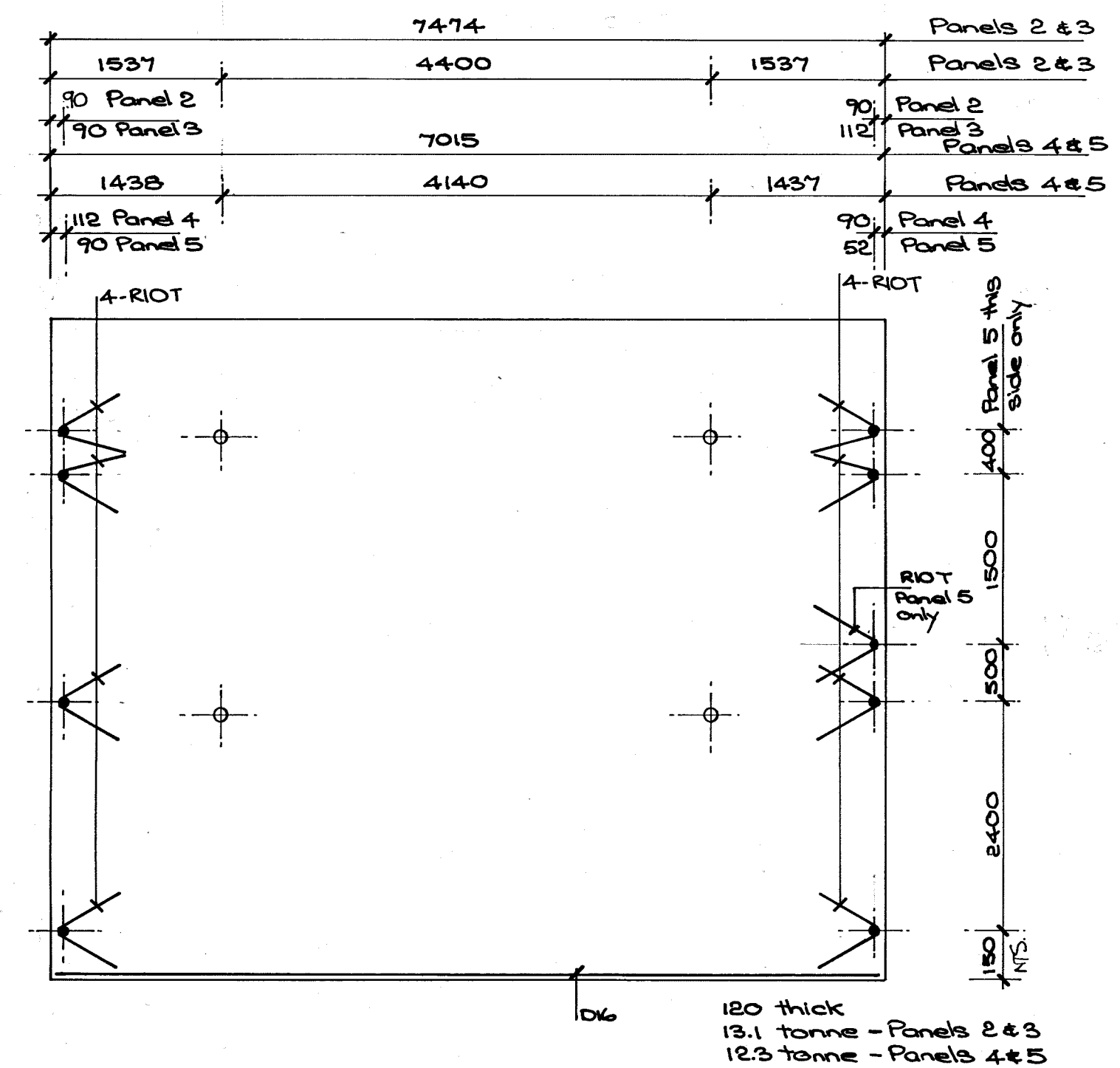
DRN	DES	CKD	APPROVED	DATE	SCALES	FOUNDATION DETAILS	SHEET	FILE
				JUNE 1993	1:20 1:10		S2 ^B	4860

A 20/1/93 changed starters from D12 to H16, Section B.
 B 30-8-93 COLUMN X AND SECTION 9 ADDED

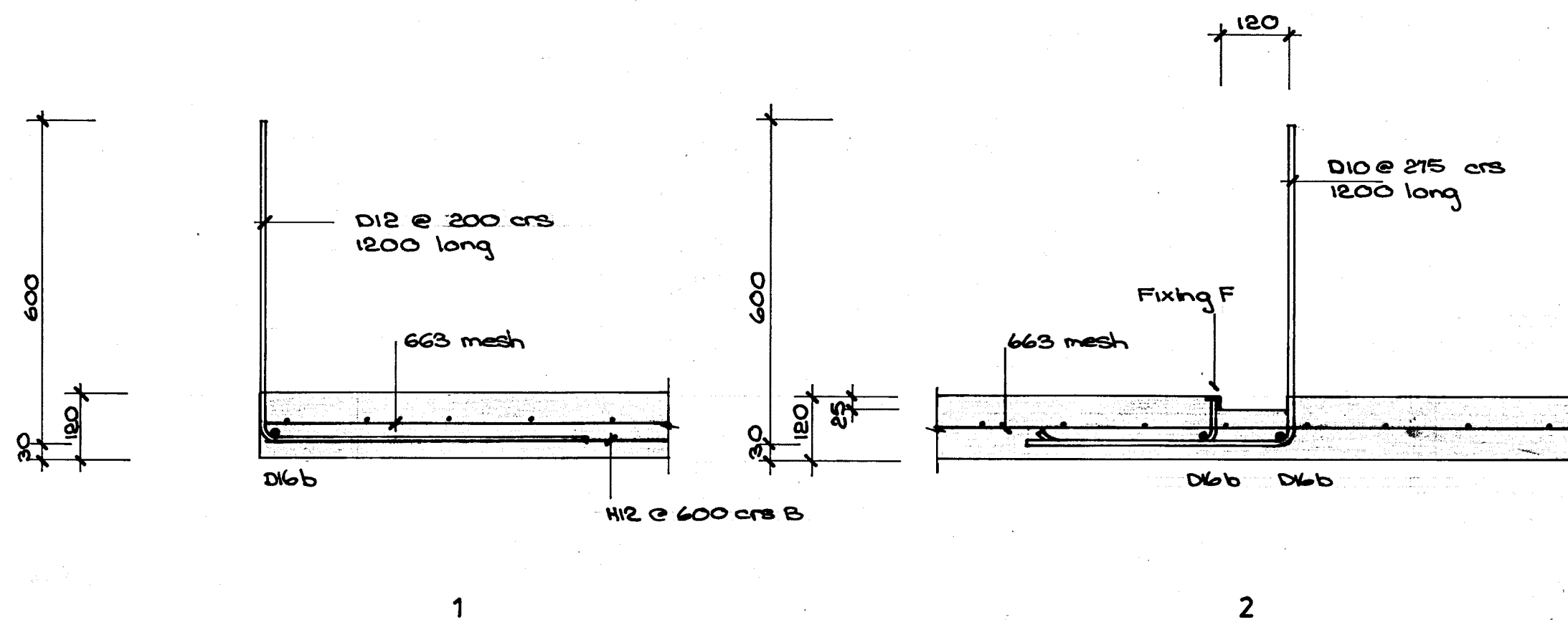




PANEL 1
PANEL 15 handed



PANELS 2 & 3
PANELS 4 & 5



Refer to sheet S3 for notes

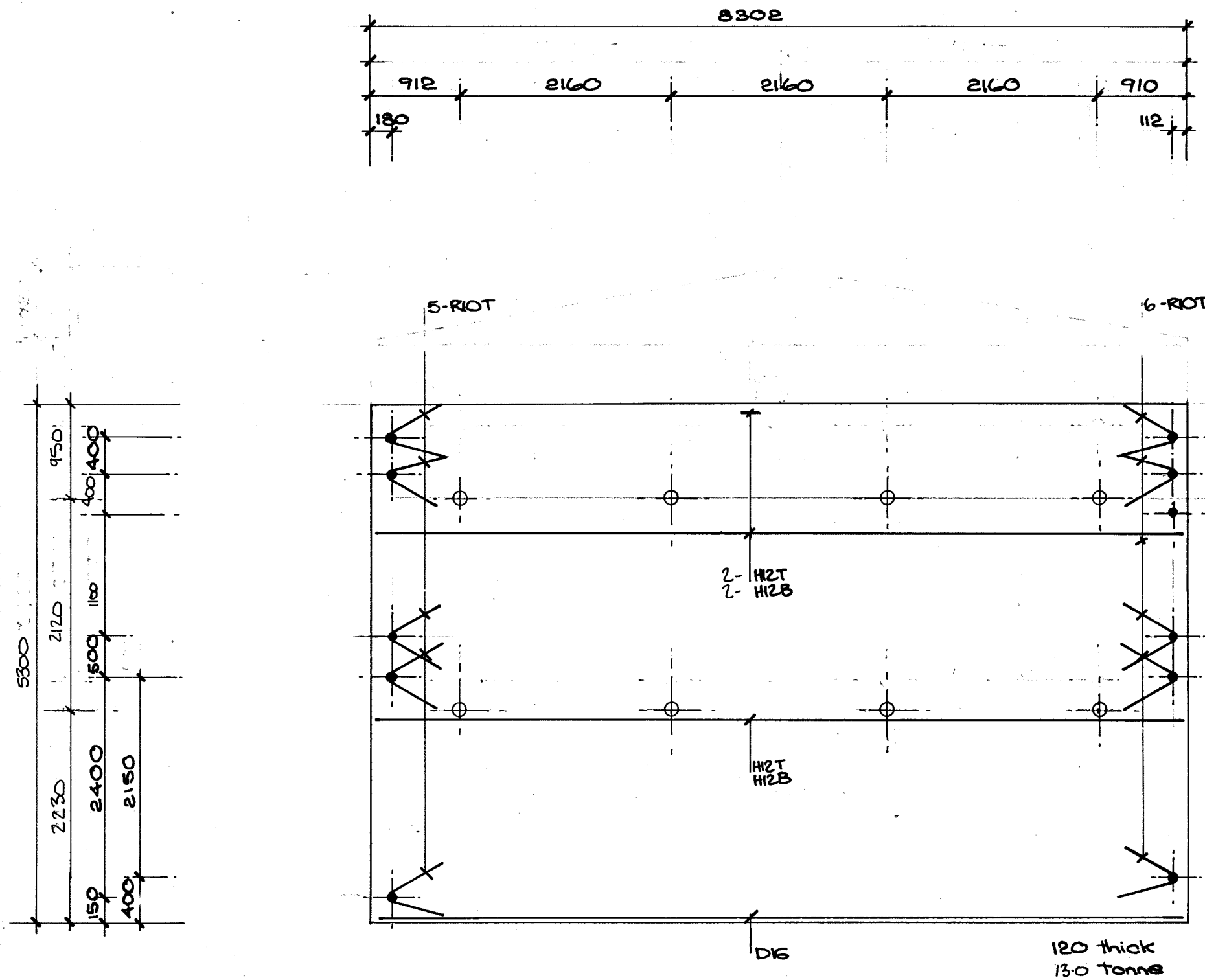
DEVELOPMENT - 121 - 123 BLENHEIM ROAD CHRISTCHURCH

DRN	W.L.S.	APPROVED	DATE	SCALES
DES			JUNE 1993	1:50
CKD				

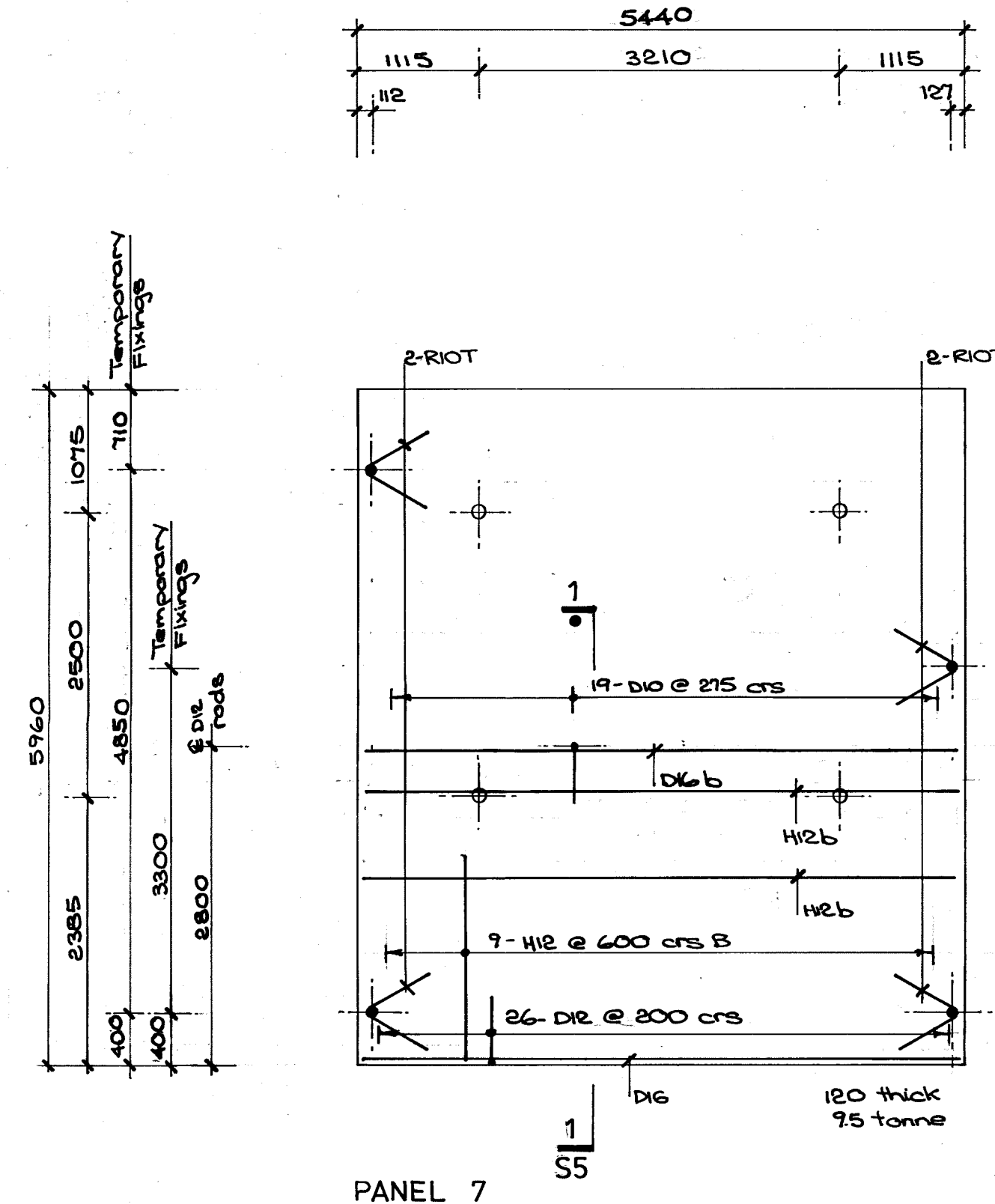
PRECAST CONCRETE
PANELS 1 - 5 & 15

SHEET	FILE
S5	4860

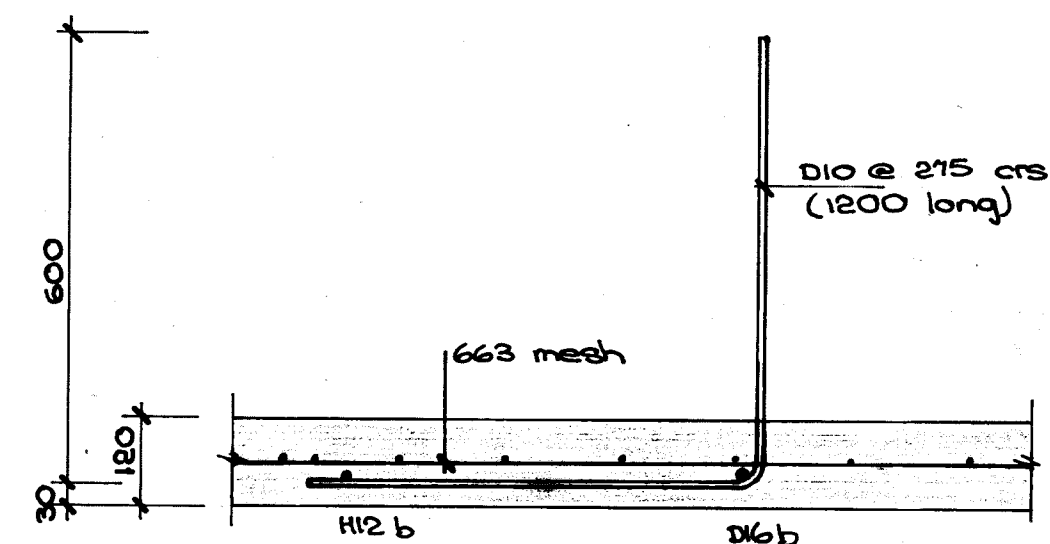
A 23-1-93 changed D12-400 starters to D10 @ 215
B 11-8-93 PANEL 1, 15 ALTERED



PANEL 6
PANEL 9 handed



PANEL 7



1

Refer to sheet S3 for notes

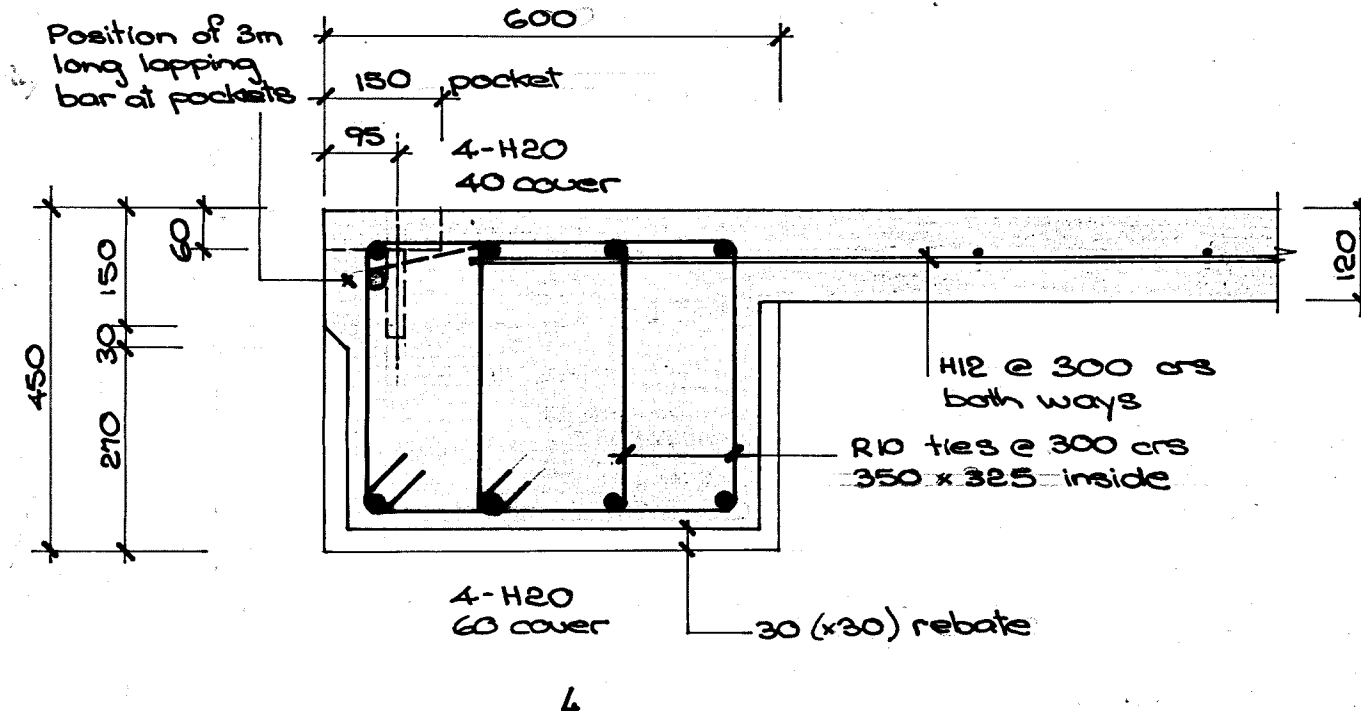
DEVELOPMENT — 121 — 123 BLENHEIM ROAD CHRISTCHURCH

DRN	W.L.S.	APPROVED	DATE	SCALES	SHEET	FILE
DES			JUNE 1993	1:50	S6 ^B	4860
CKD						

A 23-7-93 changed D12-400 starters to D10 @ 215
B 19-7-93 PANEL P6, P9 ; ALTERED TO SUIT TRANSPOWER REQUIREMENTS.



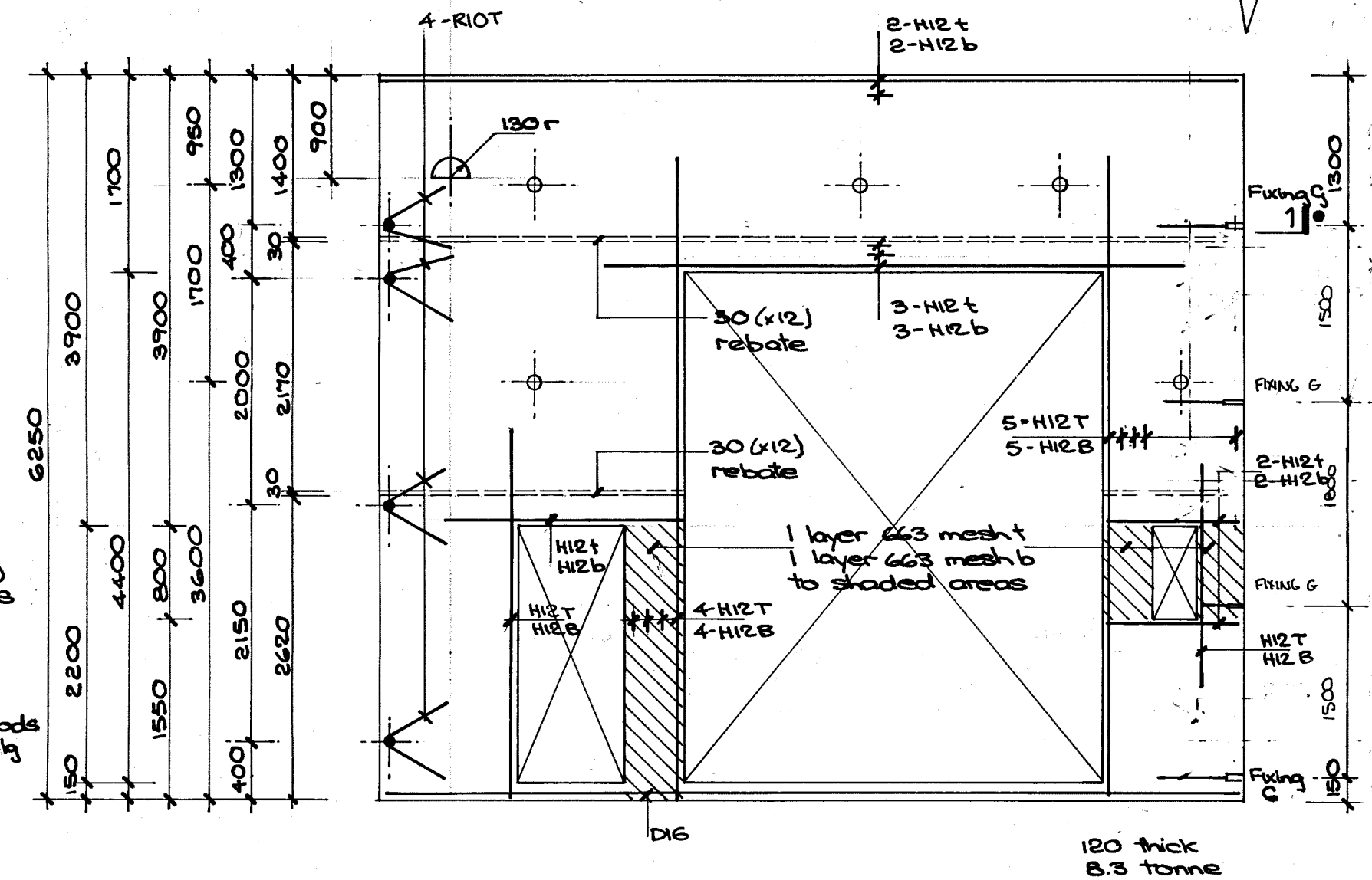
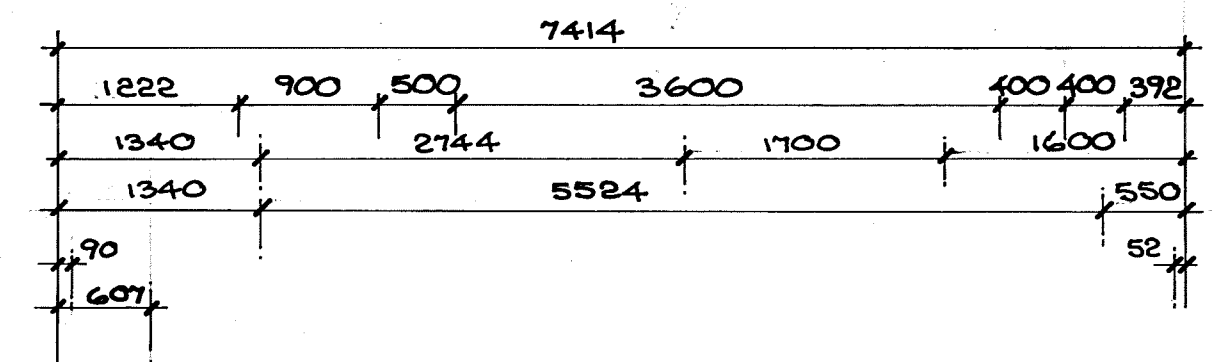
PANEL 17
PANEL 31 handed



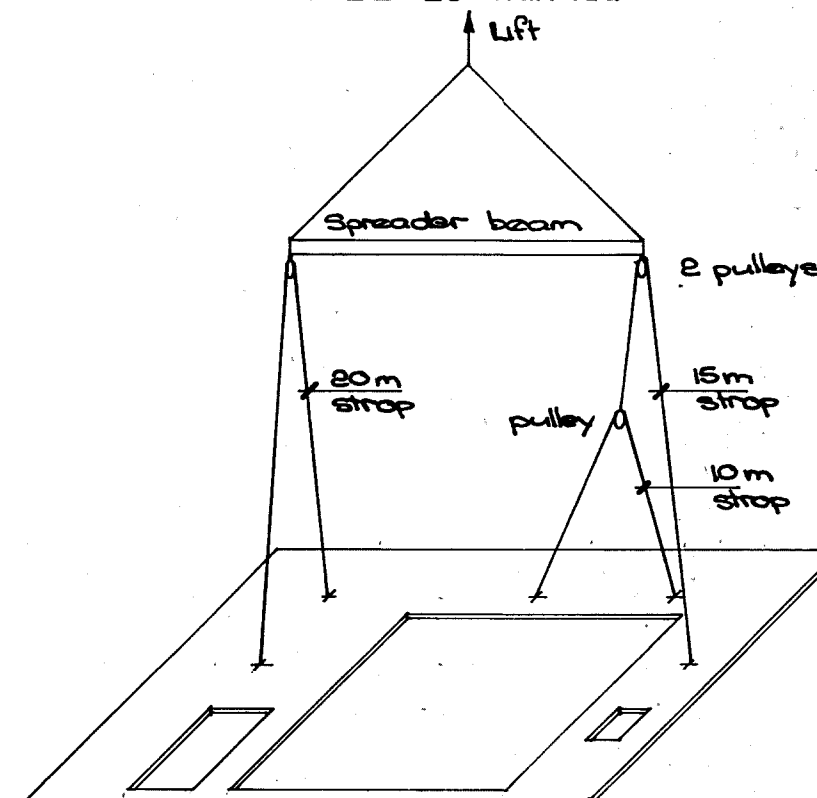
DEVELOPMENT – 121 – 123 BLENHEIM ROAD CHRISTCHURCH

DRN	W.L.S.	APPROVED	DATE	SCALES	PRECAST CONCRETE PANELS 16, 17, 31 & 32	SHEET	FILE
DES			JUNE 1993	1:50		S8c	4860
CKD							

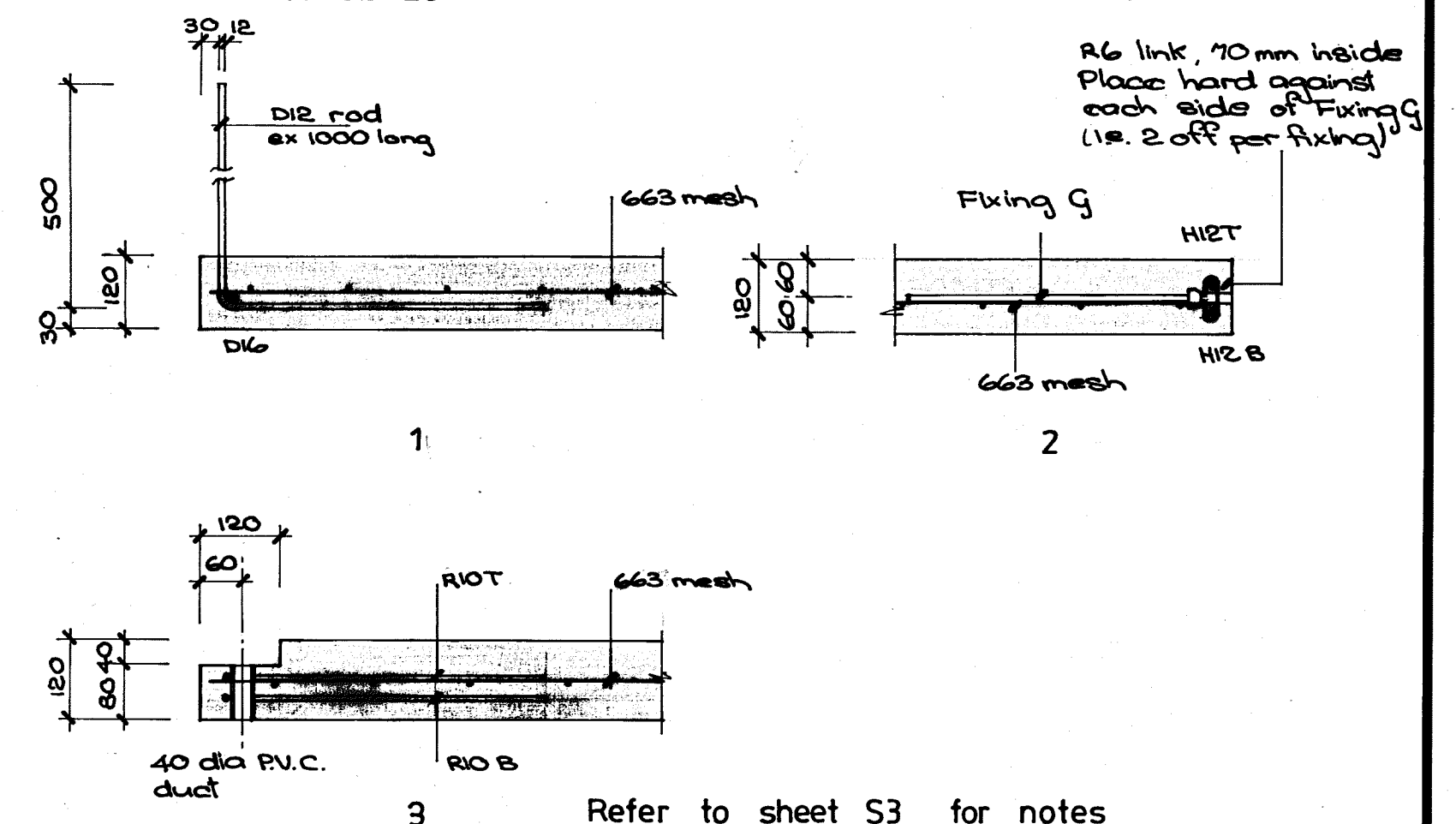
A 20/7/93 Corrected H12T to H12B on section 1.
Changed D12-400 starters to D12 @ 275
B 11-8-93 PANELS 16, 32 ALTERED, 4 FIXINGS ADDED TO SUPPORT MEZZ FLOOR



PANEL 20



LIFTING DIAGRAM PANEL 20



Refer to sheet S3 for notes

SHEET	FILE
S9 ^A	4860

A 11-8-93 PANELS 19, 20, 29 : FIXING G'S & POCKETS ADDED, FIXING H ADDED.

Appendix 2

Earthquake Damage Assessment



TM Consultants Ltd.
A. 2/7 Burdale Street.
P.O. Box 8874,
Christchurch 8440,
New Zealand
P. 03 348 6066
F. 03 348 6065
E. info@tmco.co.nz

SITE REPORT

Attn: Paul Brown

SR No : 01
File No : 140073
Date : 13/3/14
Project : 123 Blenheim Rd

POST EARTHQUAKE DAMAGE ASSESSMENT

The building at 123 Blenheim Rd is currently in use as commercial offices and retail shops. It is essentially a concrete tilt panel building with some internal portal frames. A mezzanine first floor level exists in some of the units consisting of unispan concrete slabs.

The Issues arisen from the inspection are:

LOCATION	DAMAGE	RECOMMENDED REPAIR
Foundations:	No damage to the building foundations was witnessed during the site inspection.	No Repair Recommended
Floor:	The floor slab in each unit is within 10-20mm of level. No damage was observed to the mezzanine first floor slab where connected to the concrete wall panels.	No Repair Recommended
Roof:	The roof structure appears in sound structural condition. Purlin connections appear well connected. Weathering of a panel connection where a leak has occurred was observed to the south west corner of the building. Photo 1.1	It is recommended that the leak is investigated by a competent roofer.
Walls	Significant cracking of the wall panels has been observed throughout the property. Cracks are typically between 0.1-0.5mm wide. Panel no.5 has displaced horizontally at the mid-span location by approximately 18mm due to out of plane face loading. Photos 2.1, 2.2, 2.3,2.4 Internal damage has occurred at the junctions where lightweight wall linings have moved relative to the precast panels. Photos 3.1	Inject panel cracks between 0.2 to 5mm with Sikadur-52 epoxy or similar. It is recommended this process is monitored to ensure the repair is carried out to a high standard. Patch repair areas internally.
Exterior Surroundings:	No significant damage recorded	No Repair Recommended



Photo 1.1

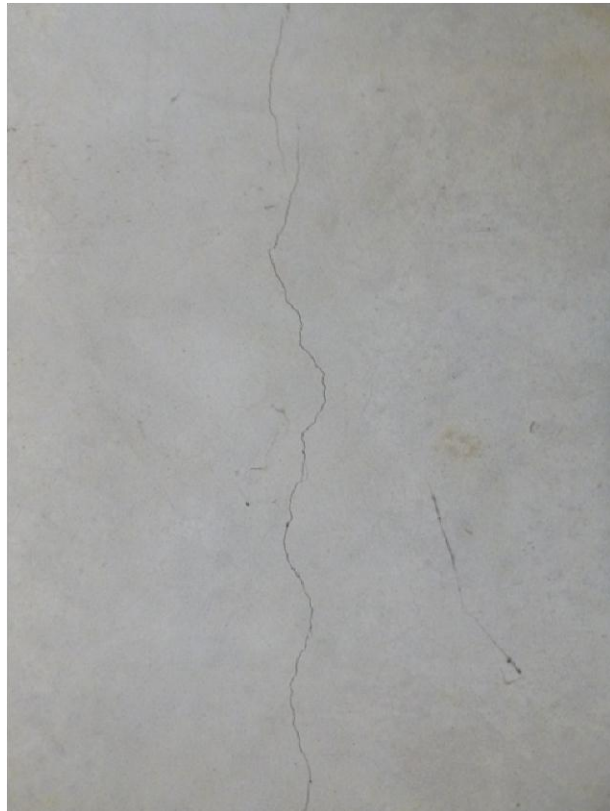


Photo 2.1



Photo 2.2

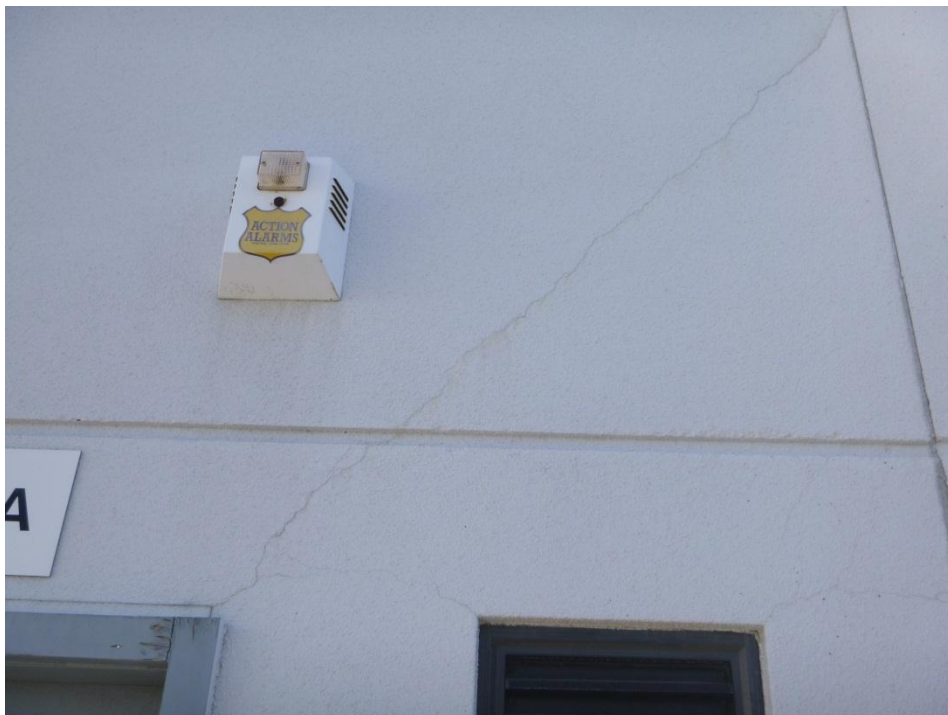


Photo 2.3

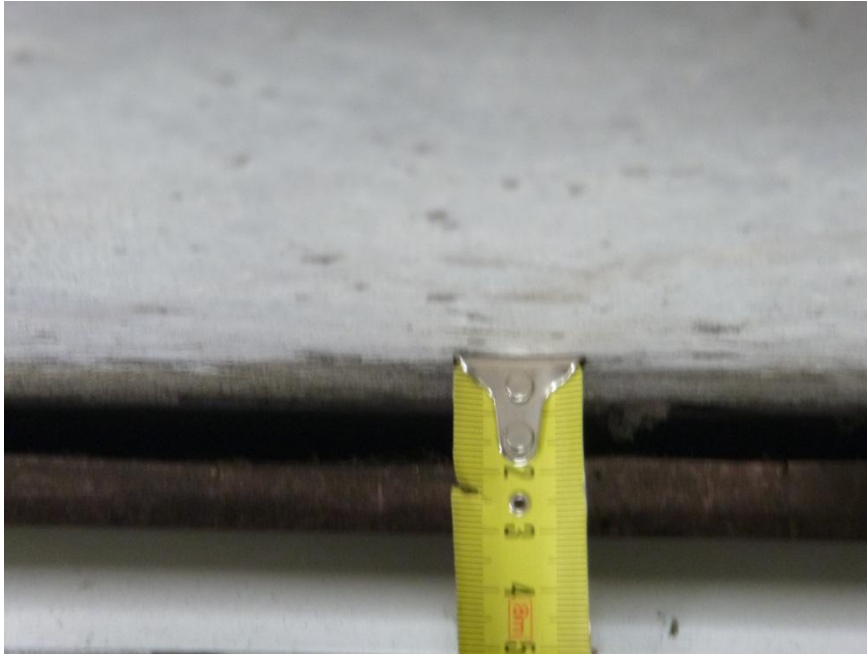


Photo 2.4



Photo 3.1

Signature:

A handwritten signature in black ink, appearing to be 'M. H. S.', written in a cursive style.

Appendix 3

IEP Standardised Report Form

Location		Building Name:		Reviewer:	
		Unit No:		CPEng No:	
		Building Address:		Company:	
		Legal Description:		Company project number:	
				Company phone number:	
		Degrees Min Sec		Date of submission:	
GPS south:		43 32 15.71		Inspection Date:	
GPS east:		172 35 59.66		Revision:	
Building Unique Identifier (CCC):				Is there a full report with this summary?	

Site		Site slope:		Max retaining height (m):	
		Soil type:		Soil Profile (if available):	
		Site Class (to NZS1170.5):			
Proximity to waterway (m, if <100m):				If Ground improvement on site, describe:	
Proximity to cliff top (m, if <100m):				Approx site elevation (m):	
Proximity to cliff base (m, if <100m):					

Building		No. of storeys above ground:		single storey = 1		Ground floor elevation (Absolute) (m):	
		Ground floor split?				Ground floor elevation above ground (m):	
		Storeys below ground:					
		Foundation type:		if Foundation type is other, describe:		Strip footings/post holes/ conc pads	
		Building height (m):		height from ground to level of uppermost seismic mass (for IEP only) (m):			
		Floor footprint area (approx):					
		Age of Building (years):				Date of design:	
		Strengthening present?				If so, when (year)?	
		Use (ground floor):				And what load level (%g)?	
		Use (upper floors):				Brief strengthening description:	
		Use notes (if required):					
		Importance level (to NZS1170.5):					

Gravity Structure		Gravity System:		rafter type, purlin type and cladding:	
		Roof:		unit type and depth (mm), topping:	
		Floors:		beam and connector type:	
		Beams:		typical dimensions (mm x mm):	
		Columns:		#N/A	
		Walls:			

Lateral load resisting structure		Lateral system along:		Note: Define along and across in		N-S Direction	
		Ductility assumed, μ :		detailed report?		note total length of wall at ground (m):	
		Period along:		enter height above at H31		estimate or calculation?	
		Total deflection (ULS) (mm):				estimate or calculation?	
		maximum interstorey deflection (ULS) (mm):				estimate or calculation?	
		Lateral system across:				E-W Direction	
		Ductility assumed, μ :				note total length of wall at ground (m):	
		Period across:		enter height above at H31		estimate or calculation?	
		Total deflection (ULS) (mm):				estimate or calculation?	
		maximum interstorey deflection (ULS) (mm):				estimate or calculation?	

Separations:		north (mm):		leave blank if not relevant	
		east (mm):			
		south (mm):			
		west (mm):			

Non-structural elements		Stairs:		describe supports:	
		Wall cladding:		describe:	
		Roof Cladding:		describe:	
		Glazing:			
		Ceilings:			
		Services(ISB):			

Available documentation		Architectural:		original designer name/date:	
		Structural:		original designer name/date:	
		Mechanical:		original designer name/date:	
		Electrical:		original designer name/date:	
		Geotech report:		original designer name/date:	

Damage Site: (refer DEE Table 4-2)		Site performance:		Describe damage:	
		Settlement:		notes (if applicable):	
		Differential settlement:		notes (if applicable):	
		Liquefaction:		notes (if applicable):	
		Lateral Spread:		notes (if applicable):	
		Differential lateral spread:		notes (if applicable):	
		Ground cracks:		notes (if applicable):	
		Damage to area:		notes (if applicable):	

Building:		Current Placard Status:			
Along		Damage ratio:		Describe how damage ratio arrived at:	
		Describe (summary):			
Across		Damage ratio:		$Damage_Ratio = \frac{(\%NBS(before) - \%NBS(after))}{\%NBS(before)}$	
		Describe (summary):			
Diaphragms		Damage?:		Describe:	
CSWs:		Damage?:		Describe:	
Pounding:		Damage?:		Describe:	
Non-structural:		Damage?:		Describe:	

Recommendations		Level of repair/strengthening required:		Describe:	
		Building Consent required:		Describe:	
		Interim occupancy recommendations:		Describe:	
Along		Assessed %NBS before e/quake:		73% #### %NBS from IEP below	
		Assessed %NBS after e/quake:		73% if IEP not used, please detail assessment methodology:	
Across		Assessed %NBS before e/quake:		73% #### %NBS from IEP below	
		Assessed %NBS after e/quake:		73%	

IEP			
Use of this method is not mandatory - more detailed analysis may give a different answer, which would take precedence. Do not fill in fields if not using IEP.			
Period of design of building (from above): 1992-2004			
Seismic Zone, if designed between 1965 and 1992:			
Design Soil type from NZS4203:1992, cl 4.6.2.2:			
along across			
Period (from above):			
(%NBS)nom from Fig 3.3:			
Note 1: for specifically design public buildings, to the code of the day: pre-1965 = 1.25; 1965-1976, Zone A = 1.33; 1965-1976, Zone B = 1.2; all else 1.0			
Note 2: for RC buildings designed between 1976-1984, use 1.2			
Note 3: for buildings designed prior to 1935 use 0.8, except in Wellington (1.0)			
along across			
Final (%NBS)nom:			
2.2 Near Fault Scaling Factor			
Near Fault scaling factor, from NZS1170.5, cl 3.1.6:			
along across			
Near Fault scaling factor (1/N(T,D), Factor A:			
2.3 Hazard Scaling Factor			
Hazard factor Z for site from AS1170.5, Table 3.3:			
Z1992, from NZS4203:1992			
Hazard scaling factor, Factor B:			
2.4 Return Period Scaling Factor			
Building Importance level (from above):			
Return Period Scaling factor from Table 3.1, Factor C:			
2.5 Ductility Scaling Factor			
Assessed ductility (less than max in Table 3.2):			
Ductility scaling factor: =1 from 1976 onwards; or = μ_p , if pre-1976, from Table 3.3:			
Ductility Scaling Factor, Factor D:			
2.6 Structural Performance Scaling Factor:			
So:			
Structural Performance Scaling Factor Factor E:			
2.7 Baseline %NBS, (NBS%) _b = (%NBS) _{nom} x A x B x C x D x E			
%NBS _b :			
Global Critical Structural Weaknesses: (refer to NZSEE IEP Table 3.4)			
3.1. Plan Irregularity, factor A:			
3.2. Vertical irregularity, Factor B:			
3.3. Short columns, Factor C:			
3.4. Pounding potential			
Pounding effect D1, from Table to right:			
Height Difference effect D2, from Table to right:			
Therefore, Factor D:			
3.5. Site Characteristics			
along across			
3.6. Other factors, Factor F			
For ≤ 3 storeys, max value = 2.5, otherwise max value = 1.5, no minimum			
Rationale for choice of F factor, if not 1:			
Detail Critical Structural Weaknesses: (refer to DEE Procedure section 6)			
List any:			
Refer also section 6.3.1 of DEE for discussion of F factor modification for other critical structural weaknesses			
3.7. Overall Performance Achievement ratio (PAR)			
along across			
4.3 PAR x (%NBS) _b :			
PAR x Baseline %NBS:			
4.4 Percentage New Building Standard (%NBS), (before)			
along across			